

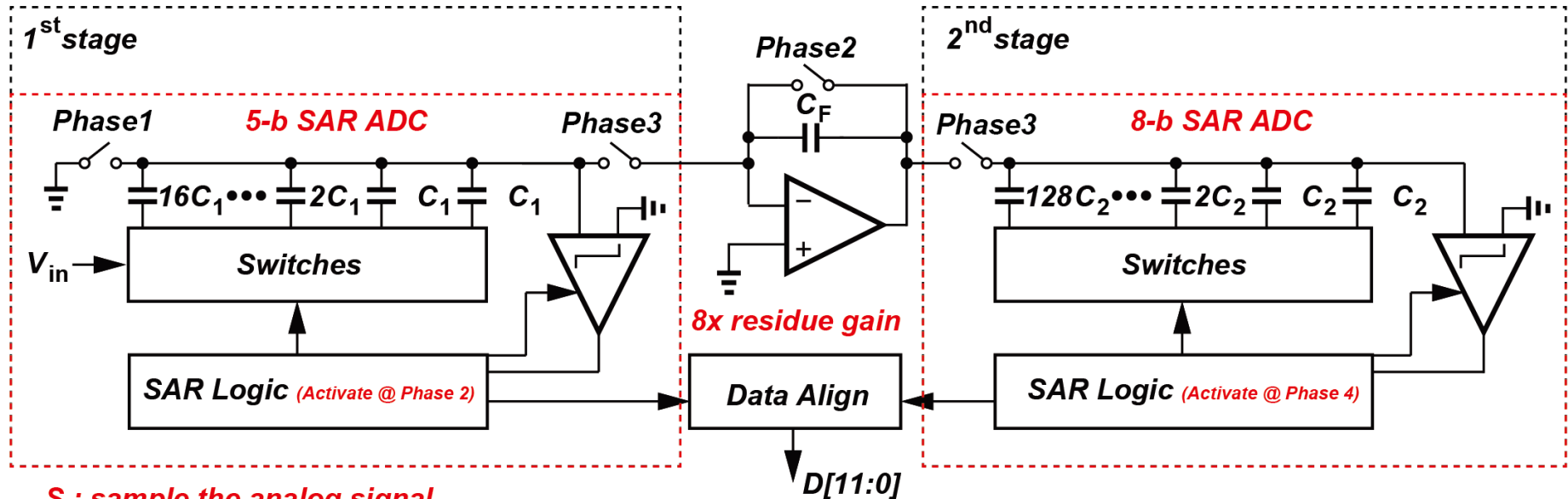
UT-Austin ADC Design ATLAS LAr Calorimeter at HL-LHC

Chen-Kai Hsu

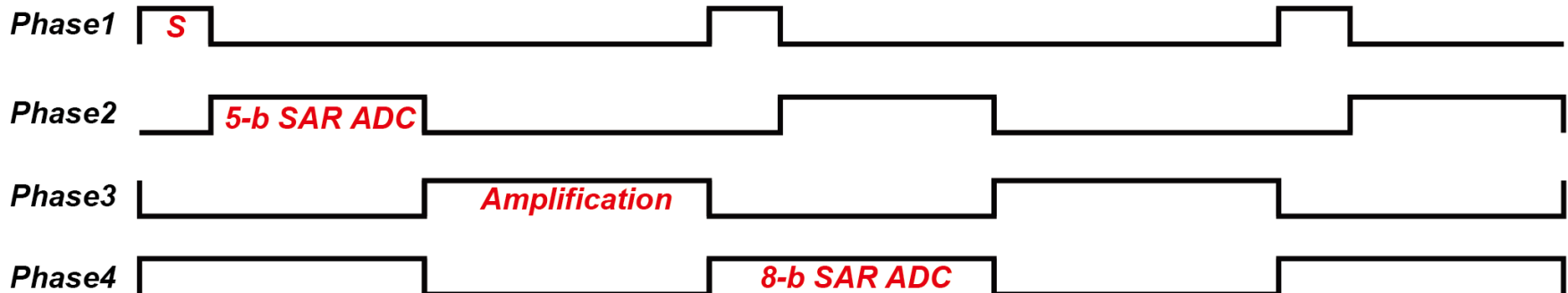
ckhsu@utexas.edu

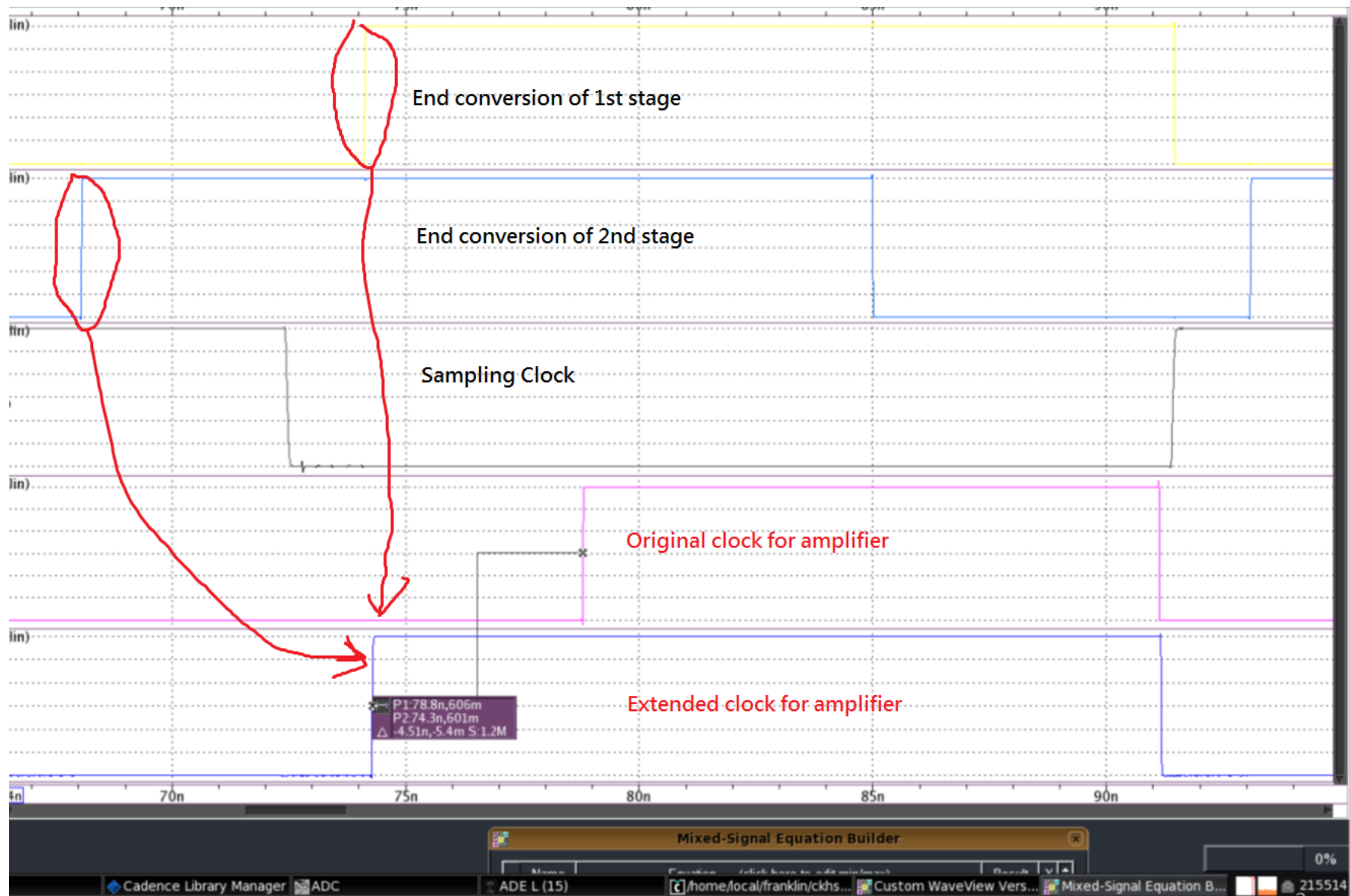
Feb 17, 2017

Adjustment on CLK Gen



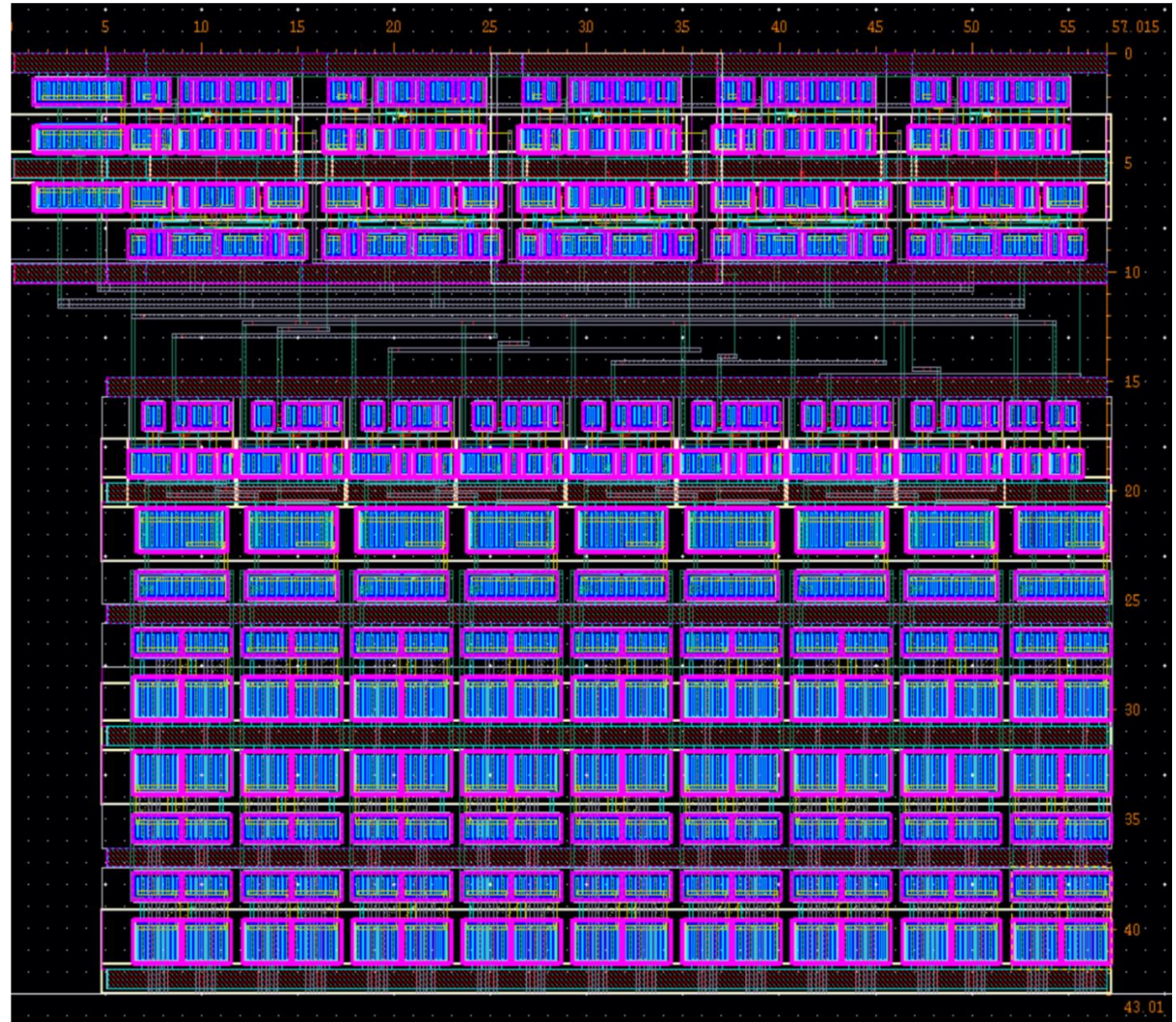
S : sample the analog signal





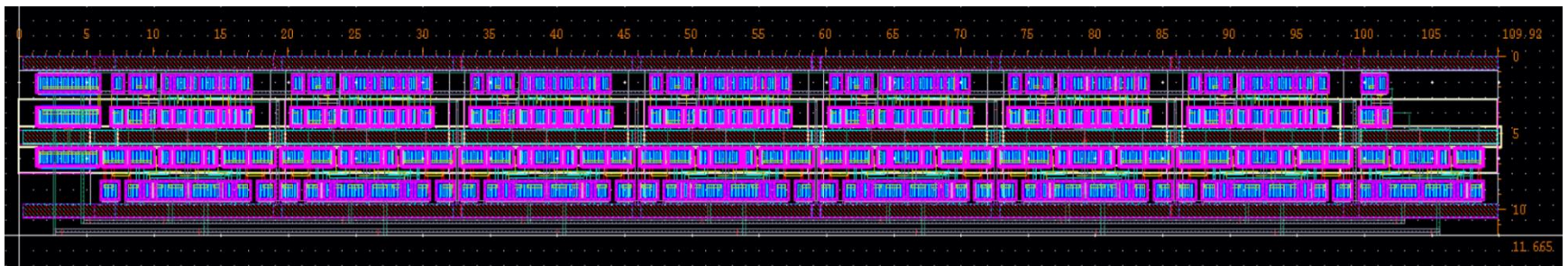
1st stage SAR logic

Area	51um*47um



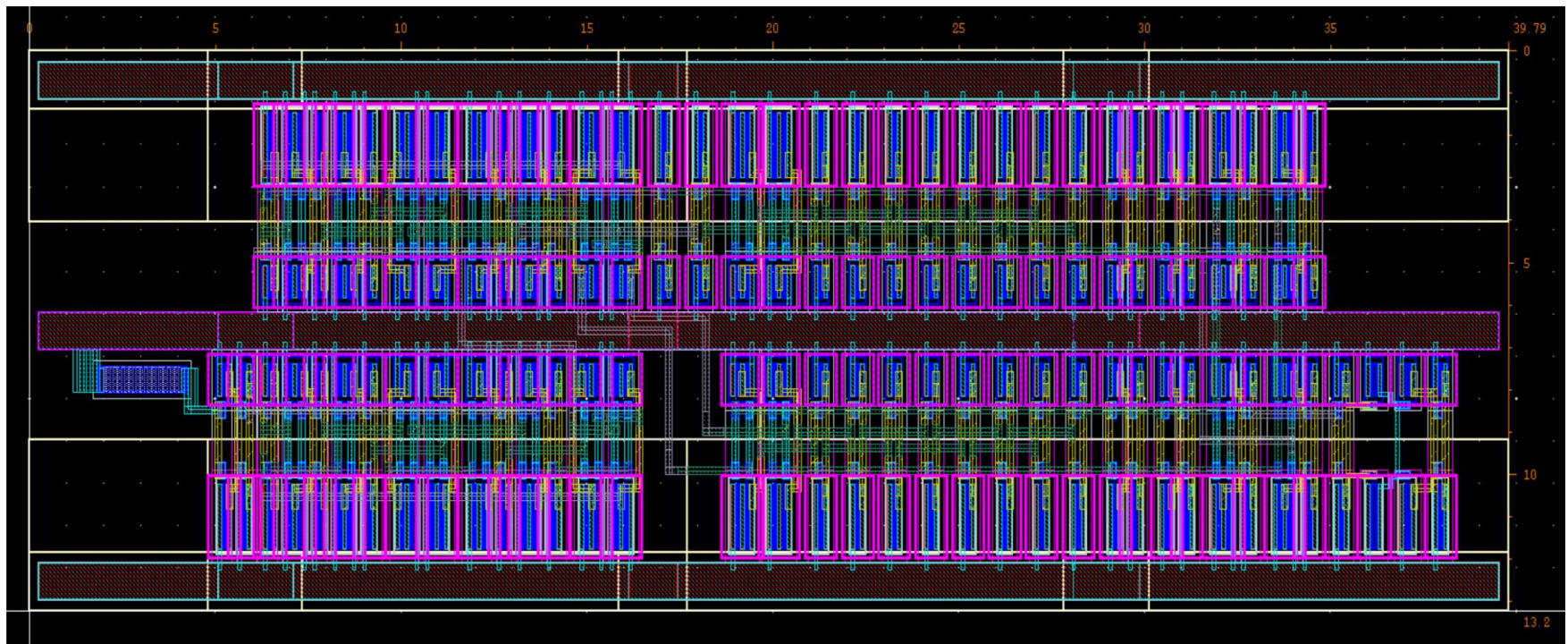
2nd stage SAR Logic

Area	109um*11um

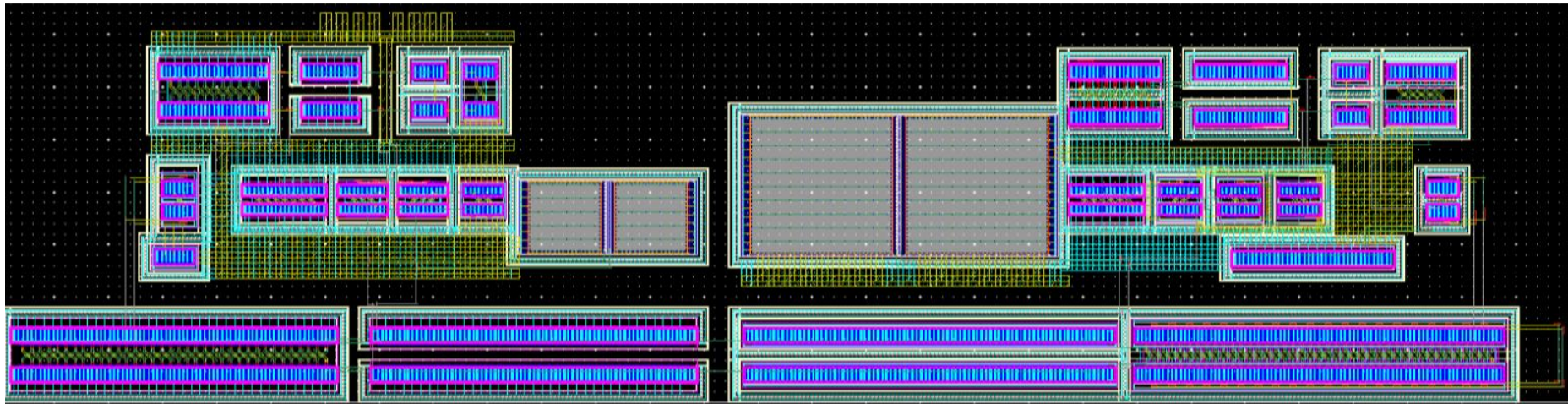


CLK_GEN

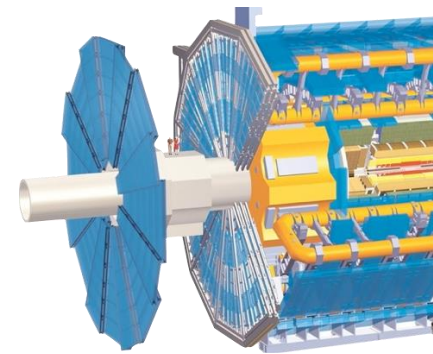
Area	39um*13um



Amplifier(not finished)



Now~2/28	March
1st Sar Logic 2nd Sar Logic CLK_GEN Comparator Amplifier Bootstrap SW DAC	Whole Chip routing & post-sim

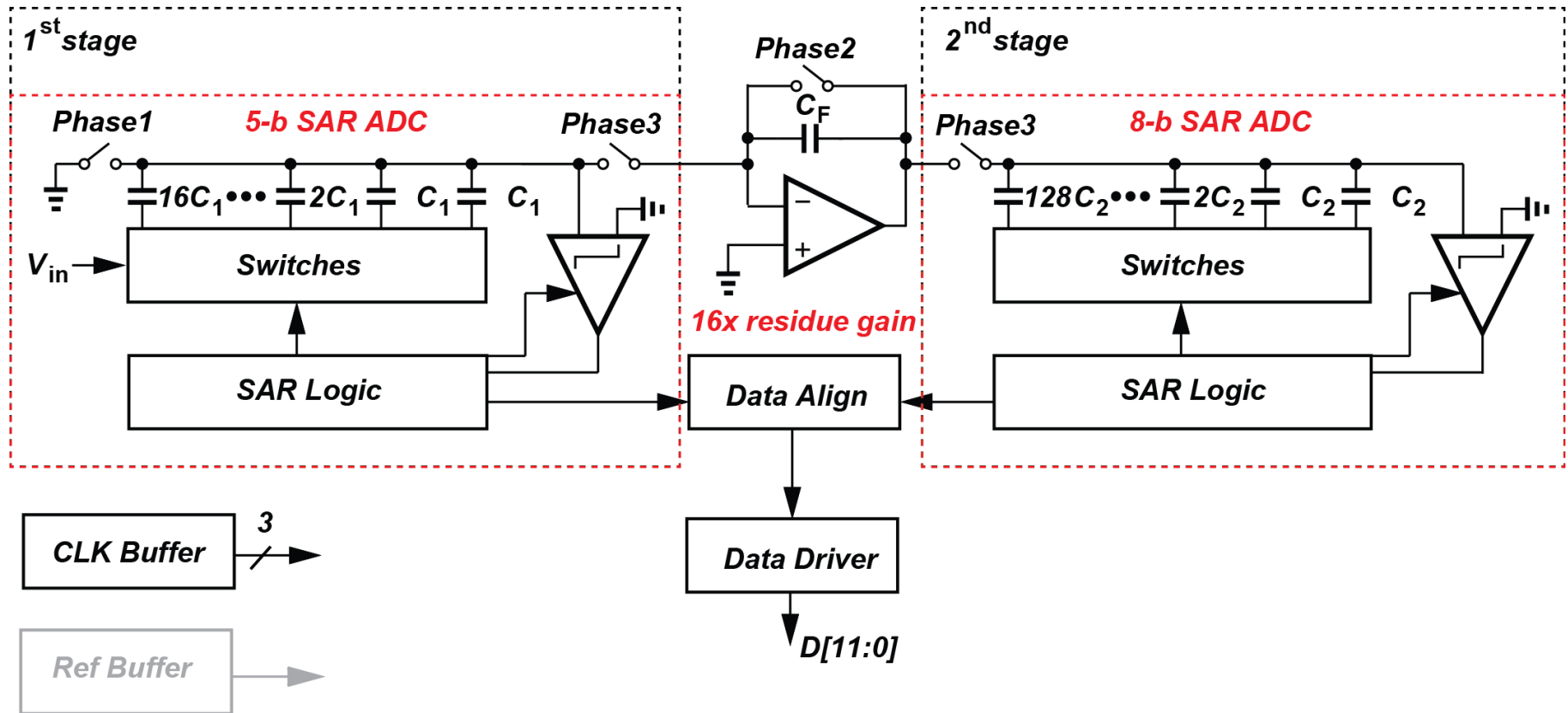


UT-Austin ADC Design ATLAS LAr Calorimeter at HL-LHC

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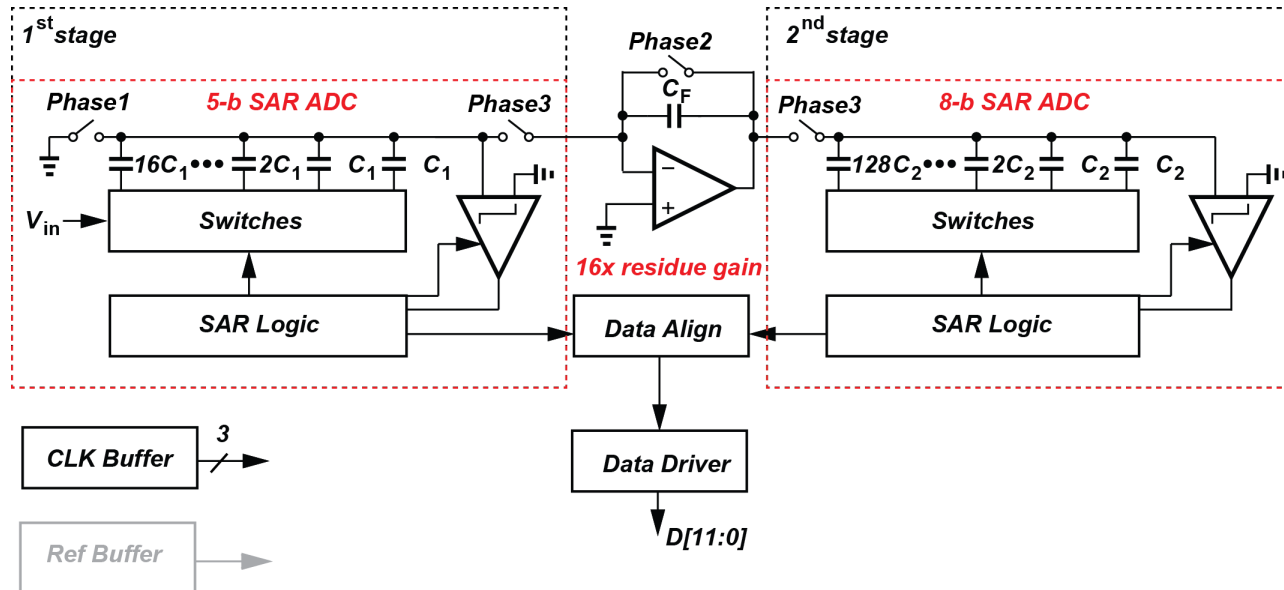
ckhsu@utexas.edu

Jan 27, 2017



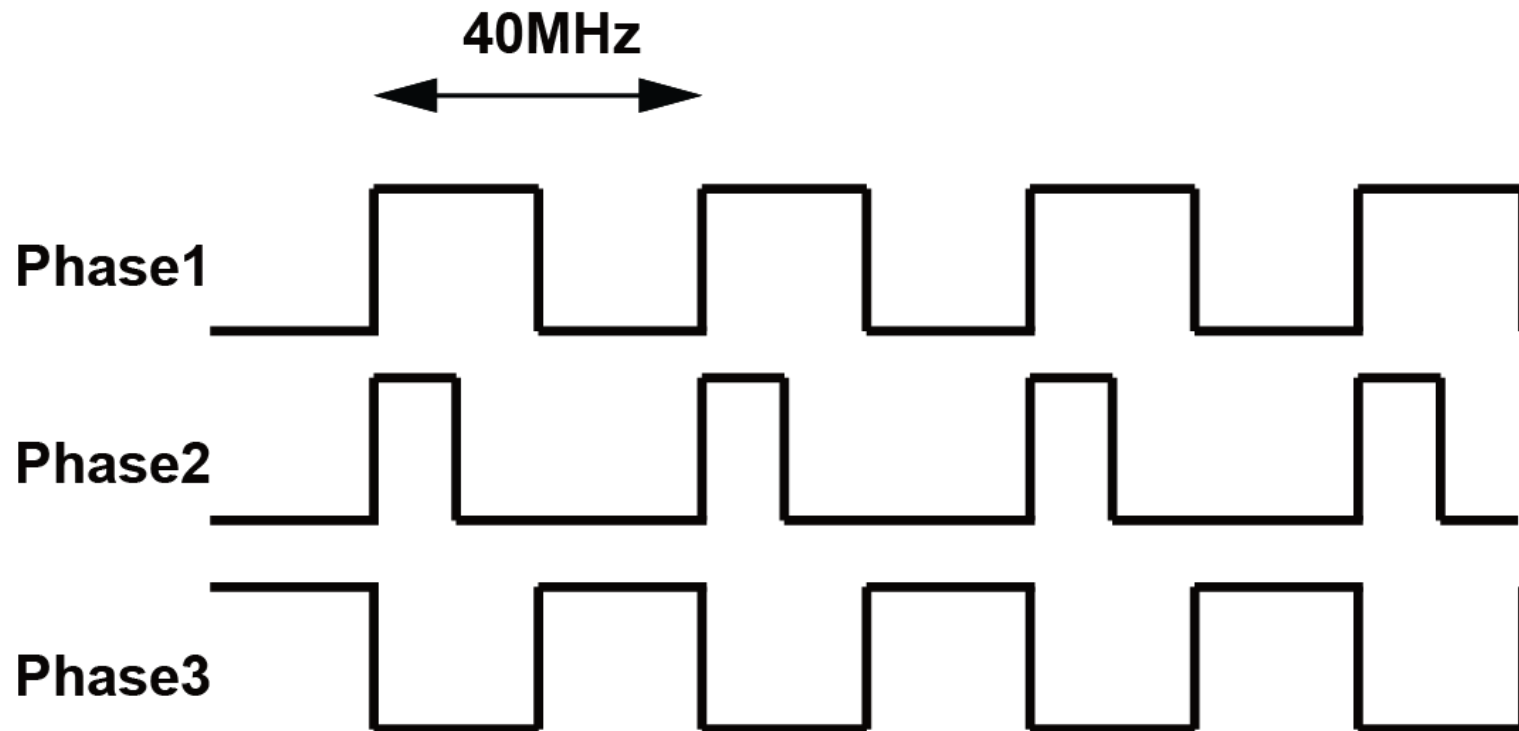


This ADC	Specification	OPAMP	Specification
Supply Voltage	1.2 V	Supply Voltage	1.2 V
Technology	TSMC 65LP	Technology	TSMC 65LP
Sampling Rate	40MS/s	DC Gain	87 dB
ENOB	11.66 bit	GBW	2.1 GHz
Power	4mW (no Ref Buffer)	Phase Margin	80 degree
Input capacitance	2pF single ended	Power	1.8 mW

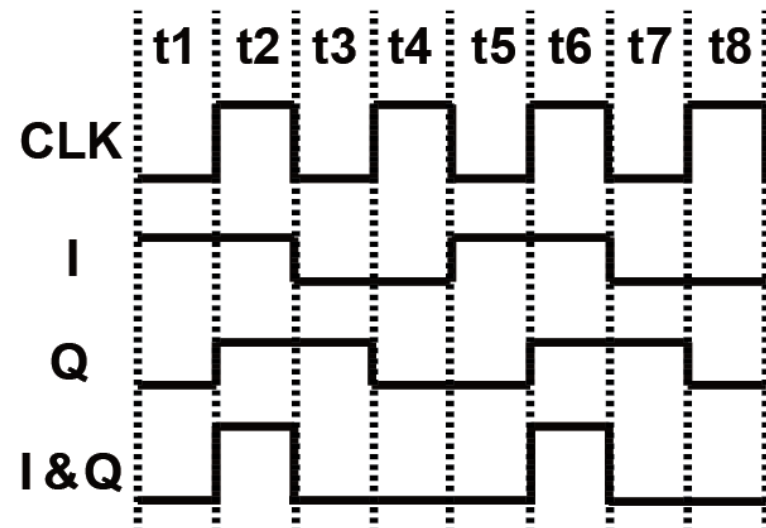
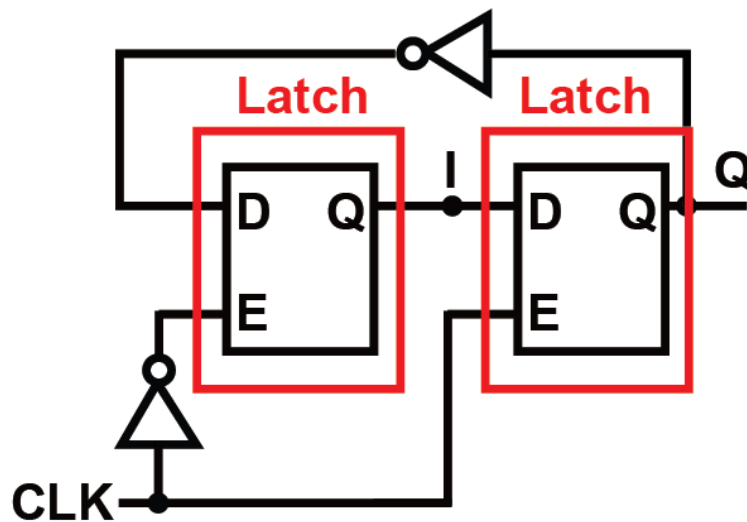
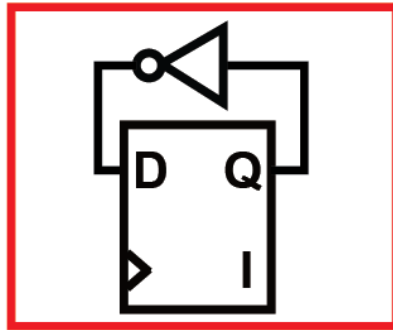


	Now~2/26	2/26~3/26	3/26~4/26
Layout	Stage1 OPAMP	Stage 2 Clk buffer	Whole Chip
verification	presim(ADC) Stage1	stage2 with stage1	Whole Chip

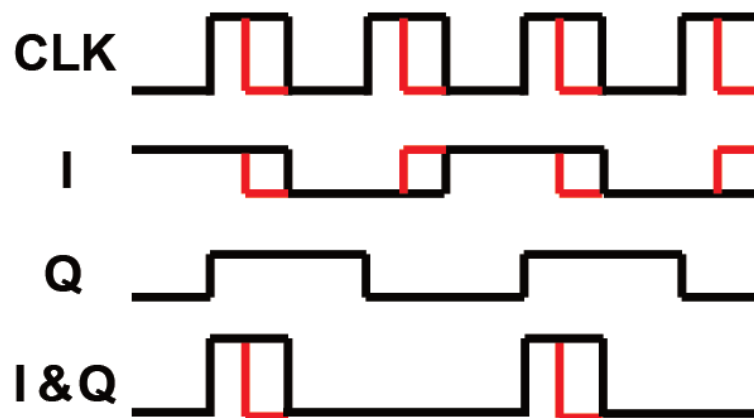
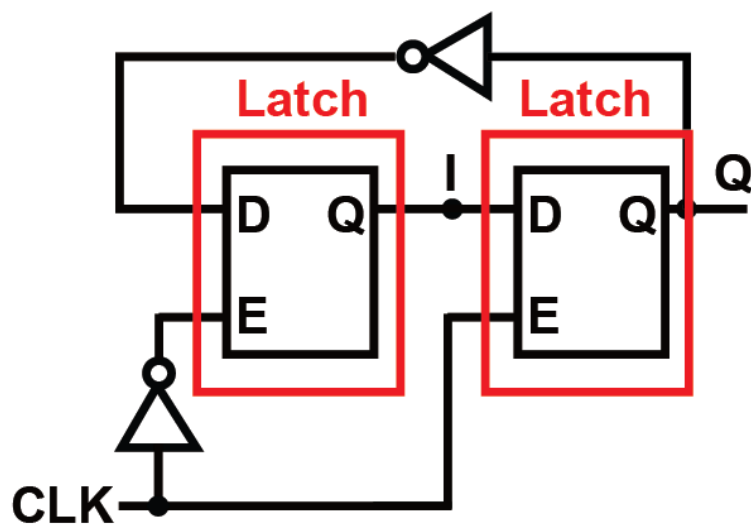
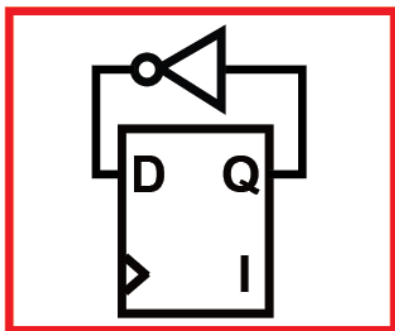
- In this ADC, three kinds of clock are used.

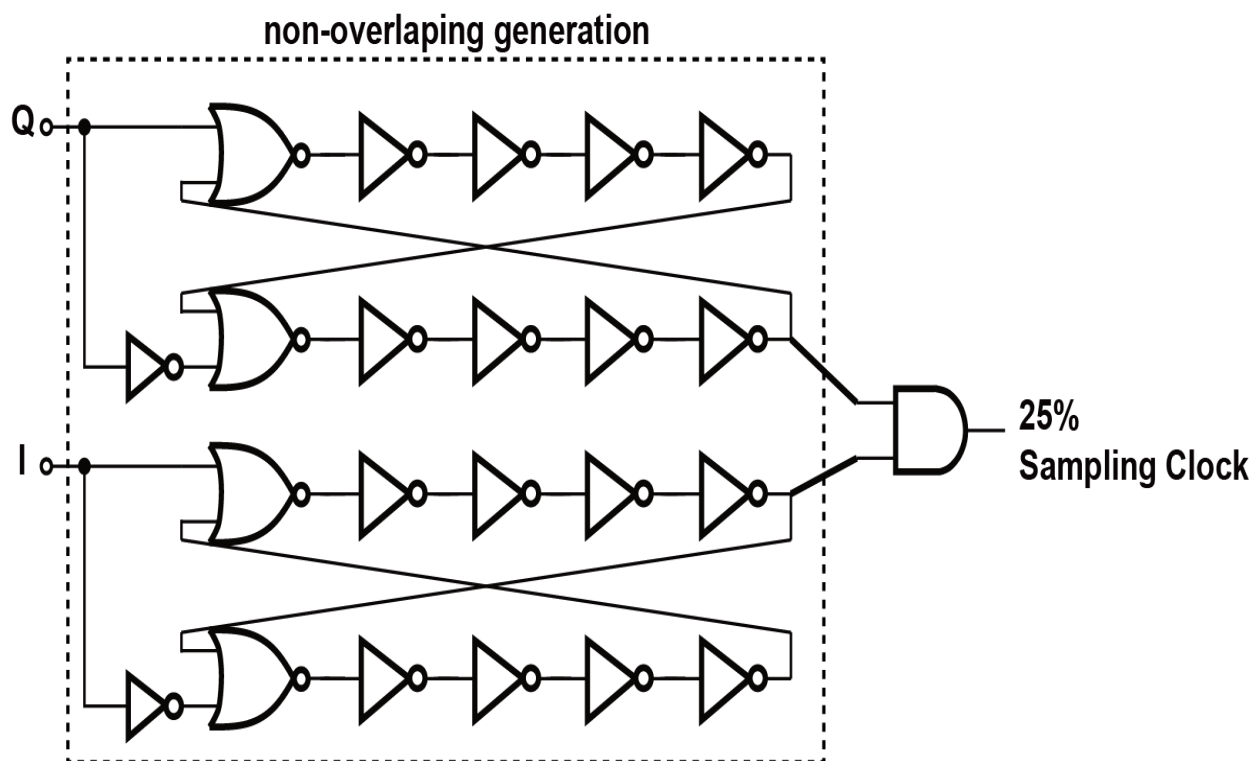
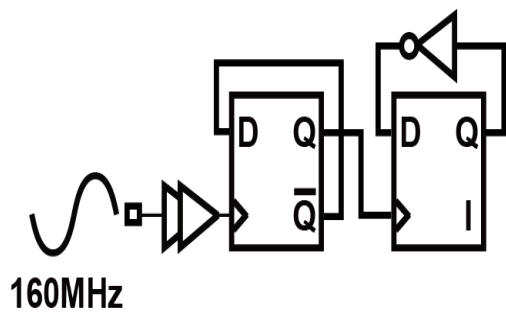


Frequency Divider



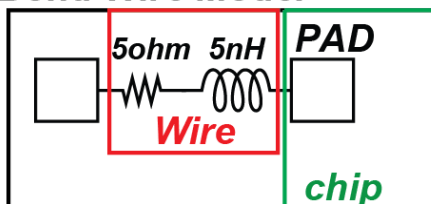
Frequency Divider



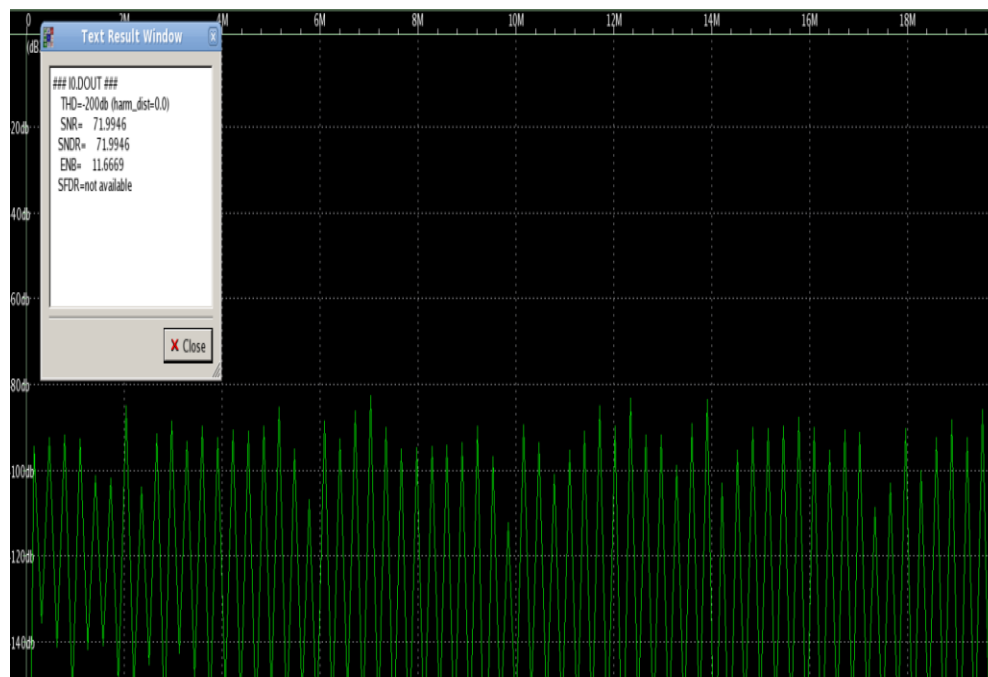
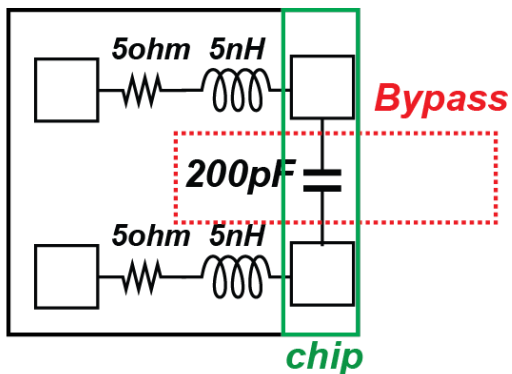


Bonding wire simulation

Bond Wire Model

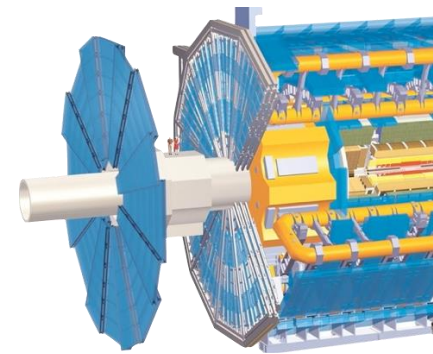


For Reference Voltage



Tapeout date?

Gustaff	John	Estimated Chip Back
	February 01	
February 15		
	February 22	
	April 05	
	April 26	July 12
May 25	May 25	August 16



UT-Austin ADC Design ATLAS LAr Calorimeter at HL-LHC

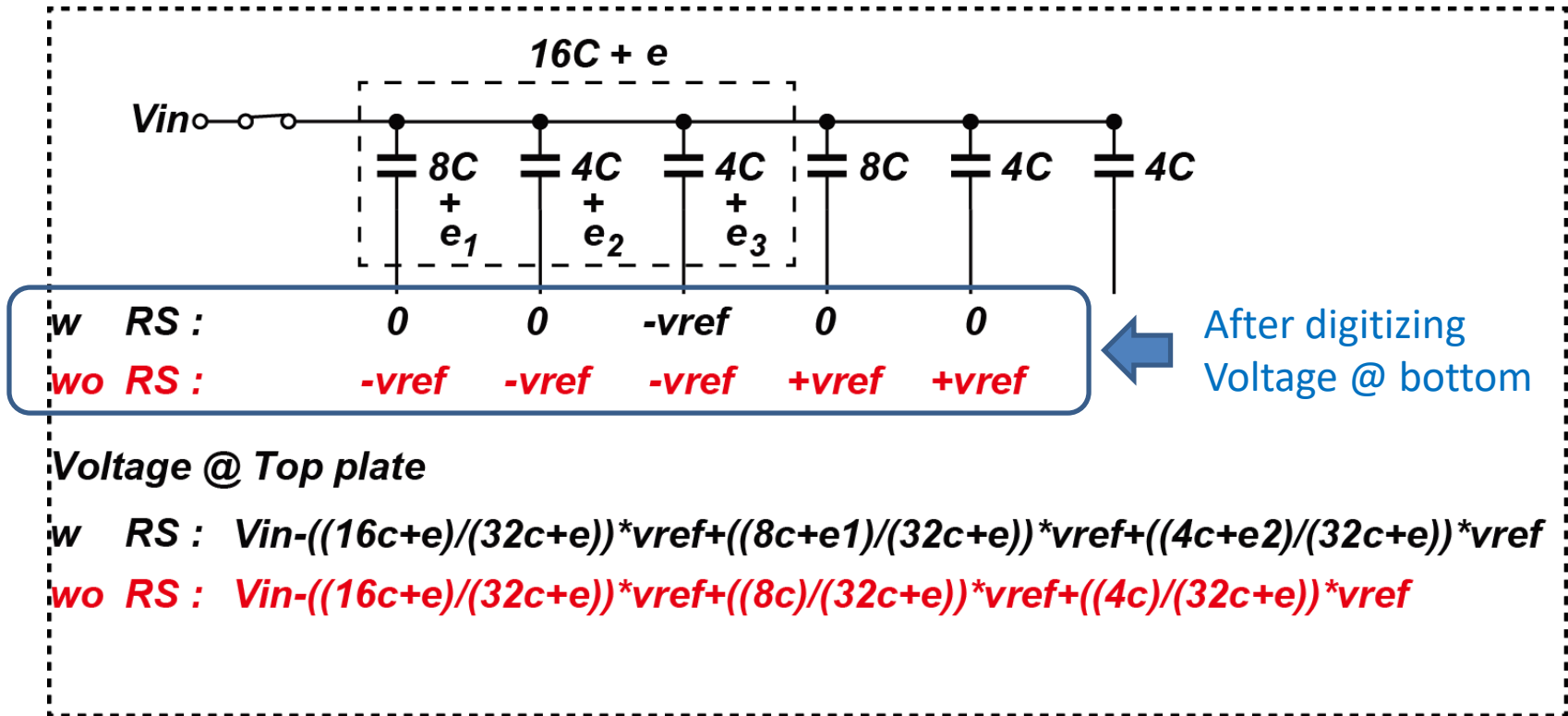
Chen-Kai Hsu

ckhsu@utexas.edu

Dec 20, 2016

Switching back

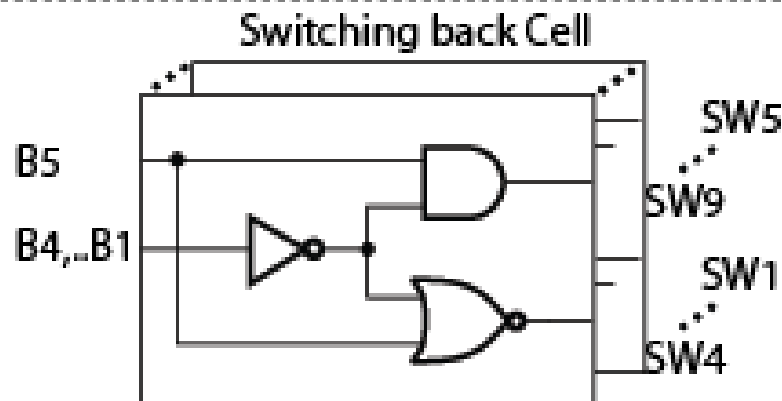
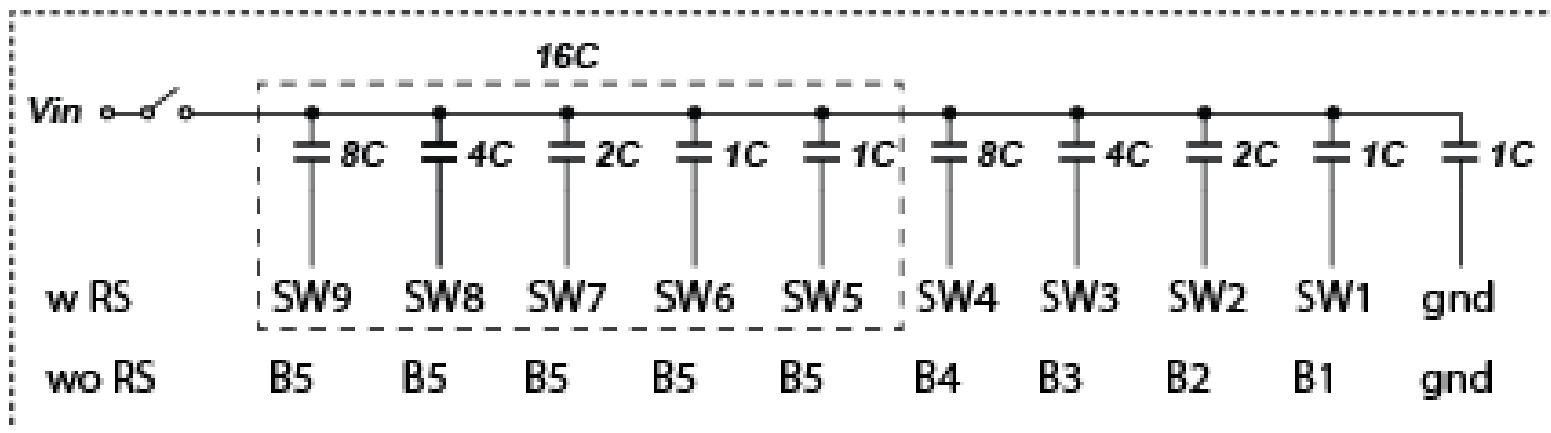
- Digital Sequence : 100



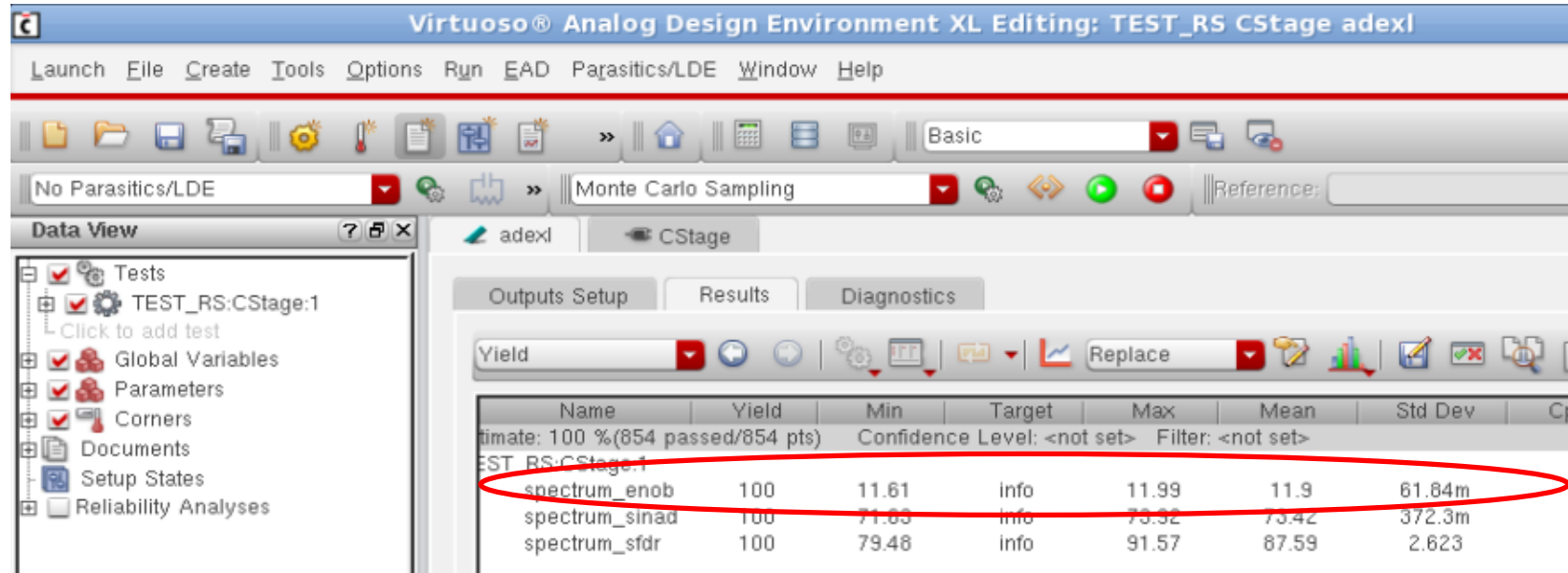
- Remember that e equals to $e_1 + e_2 + e_3$

Switching back(cont.)

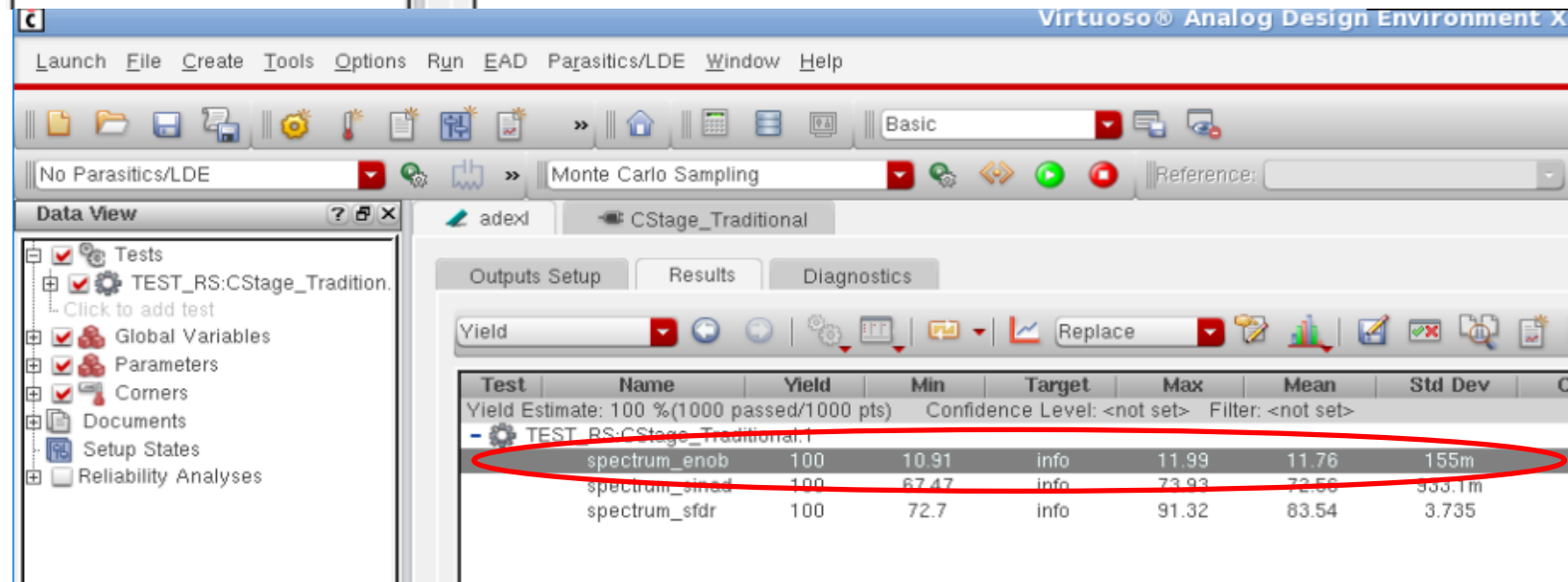
- B5 controls SW9, SW8... SW5 if without switching back.

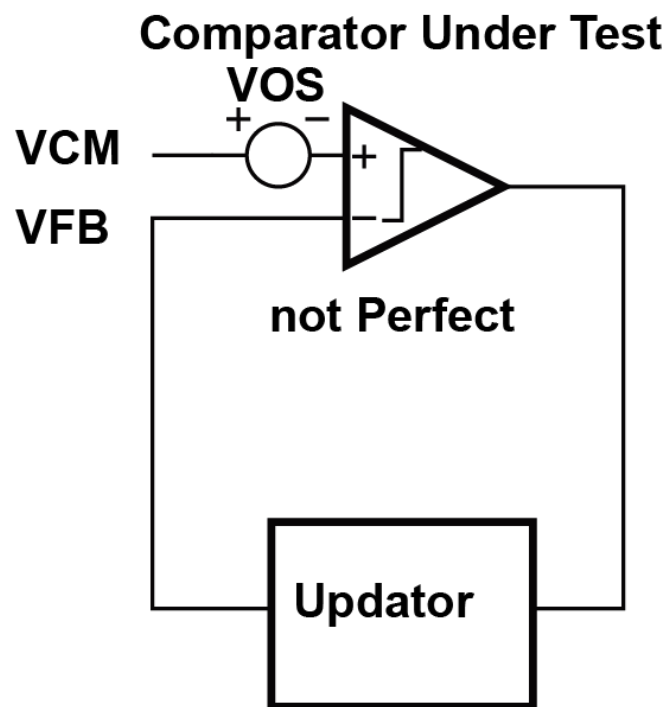
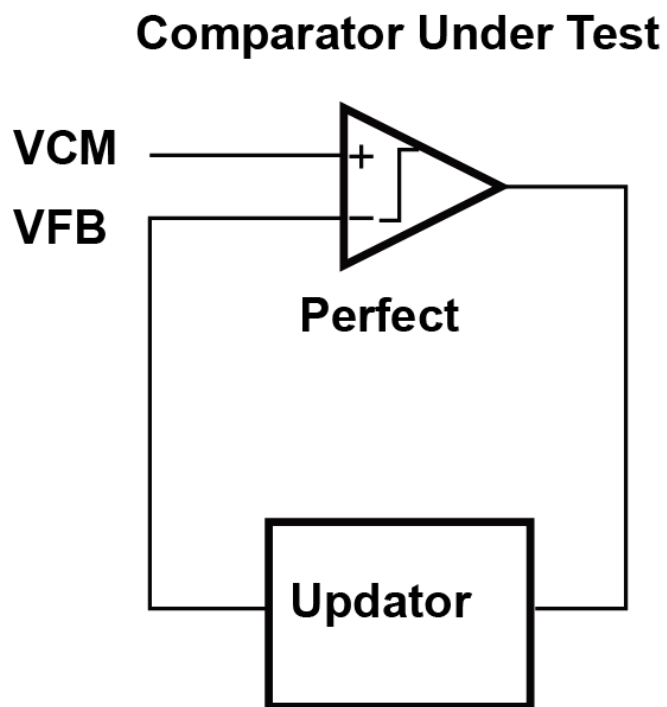


With
Reverse
switching



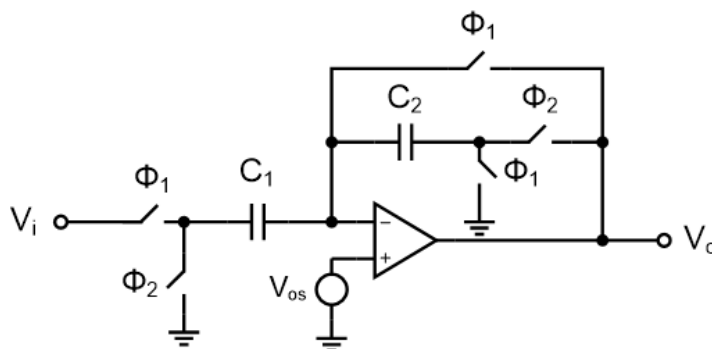
Without
Reverse
switching





Test	Name	Yield	Min	Target	Max	Mean	Std Dev	Ci
Yield Estimate: 100 %(1000 passed/1000 pts) Confidence Level: <not set> Filter: <not set>								
- ADC65LP:CLatchOffsetSimulation:1								
	VOS	100	-15.63m	info	14.31m	326.8u	4.644m	

- Opamp offset canceled out by auto-zero technique.



$$\sum Q(\phi_1) = [V_i(n) - V_{os}]C_1 - V_{os}C_2 \quad (1)$$

$$\sum Q(\phi_2) = -V_{os}C_1 + [V_o(n) - V_{os}]C_2 \quad (2)$$

$$H(z) = \frac{V_o(z)}{V_i(z)} = \frac{C_1}{C_2}$$

- Most of corners meet our requirement.

Parameter	C0_0	C0_1	C0_2	C0_3	C0_4	C0_5	C0_6	C0_7	C0_27	C0_28	C0_29	C0_30	C0_31	C0_32	C0_33	C0_34	C0_35
Model Group	TT	TT	TT	TT	TT	TT	TT	TT	FS	FS	FS	FS	FS	FS	FS	FS	FS
VDD	1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
temperature	-20	27	80	-20	27	80	-20	27	-20	27	80	-20	27	80	-20	27	80

Output	C0_0	C0_1	C0_2	C0_3	C0_4	C0_5	C0_6	C0_7	C0_27	C0_28	C0_29	C0_30	C0_31	C0_32	C0_33	C0_34	C0_35
gbw	3.291G	2.83G	2.425G	3.408G	3.015G	2.643G	3.53G	3.151G	3.12G	2.769G	2.274G	3.427G	2.921G	2.5G	3.501G	3.055G	2.658G
gain	81.96	81.32	75.74	90.93	88	82.83	93.39	88.32	33.79	81.93	72.95	88.2	85.28	79.84	90.86	85.73	81.03

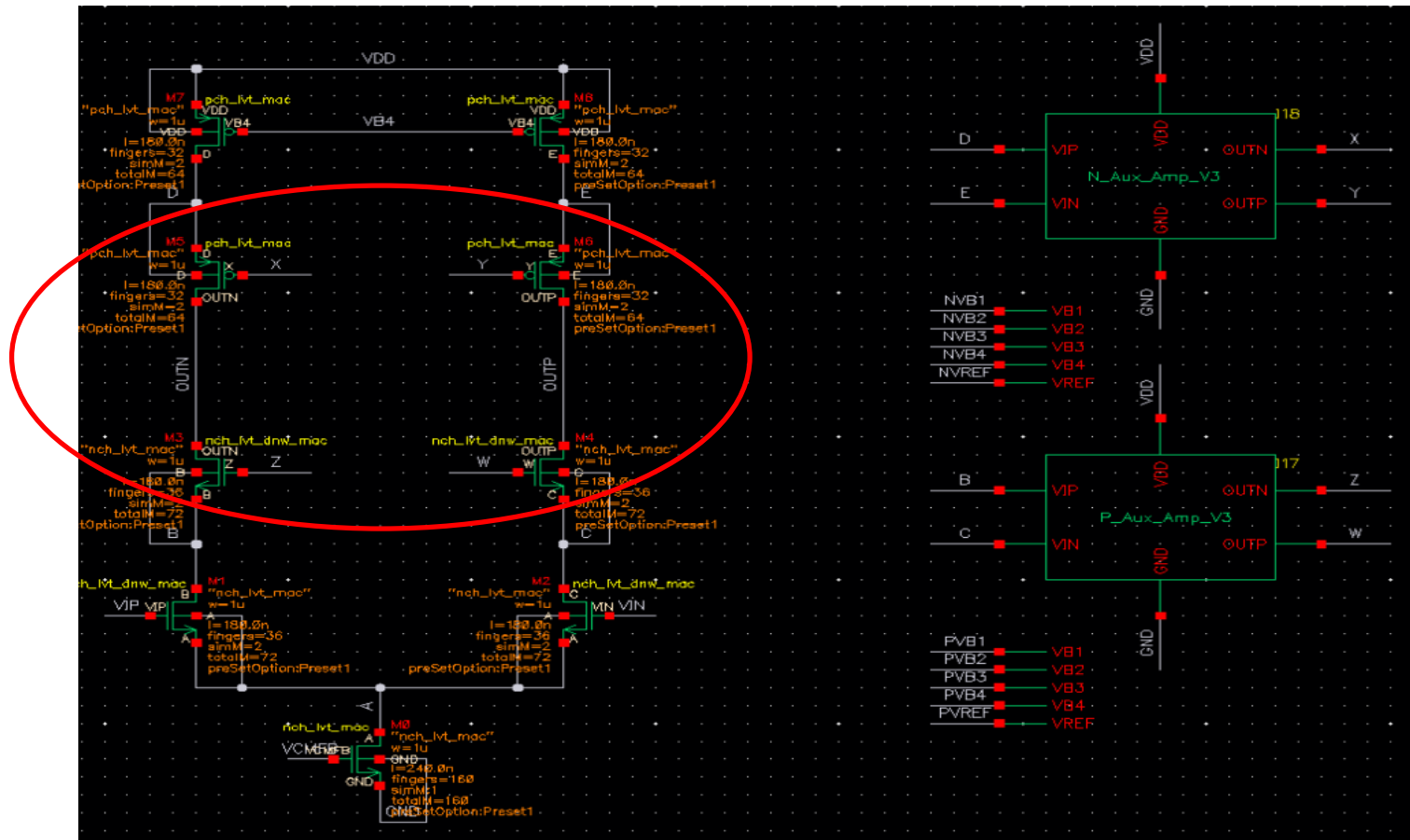
Parameter	C0_18	C0_19	C0_20	C0_21	C0_22	C0_23	C0_24	C0_25	C0_26	C0_36	C0_37	C0_38	C0_39	C0_40	C0_41	C0_42	C0_43	C0_44
Model Group	SS	SS	SS	SS	SS	SS	SS	SS	SS	SF	SF	SF	SF	SF	SF	SF	SF	SF
VDD	1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32	1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
temperature	-20	27	80	-20	27	80	-20	27	80	-20	27	80	-20	27	80	-20	27	80

Output	C0_18	C0_19	C0_20	C0_21	C0_22	C0_23	C0_24	C0_25	C0_26	C0_36	C0_37	C0_38	C0_39	C0_40	C0_41	C0_42	C0_43	C0_44
gbw	3.084G	2.878G	2.329G	3.055G	3.023G	2.604G	3.213G	3.147G	2.742G	2.901G	2.904G	2.577G	3.016G	3.098G	2.763G	3.244G	3.24G	2.899G
gain	33.75	81.55	76.65	53.99	90.9	85.98	61.82	92.34	86.83	36.44	79.3	76.38	32.43	88.03	84.2	64.74	89.4	84.92

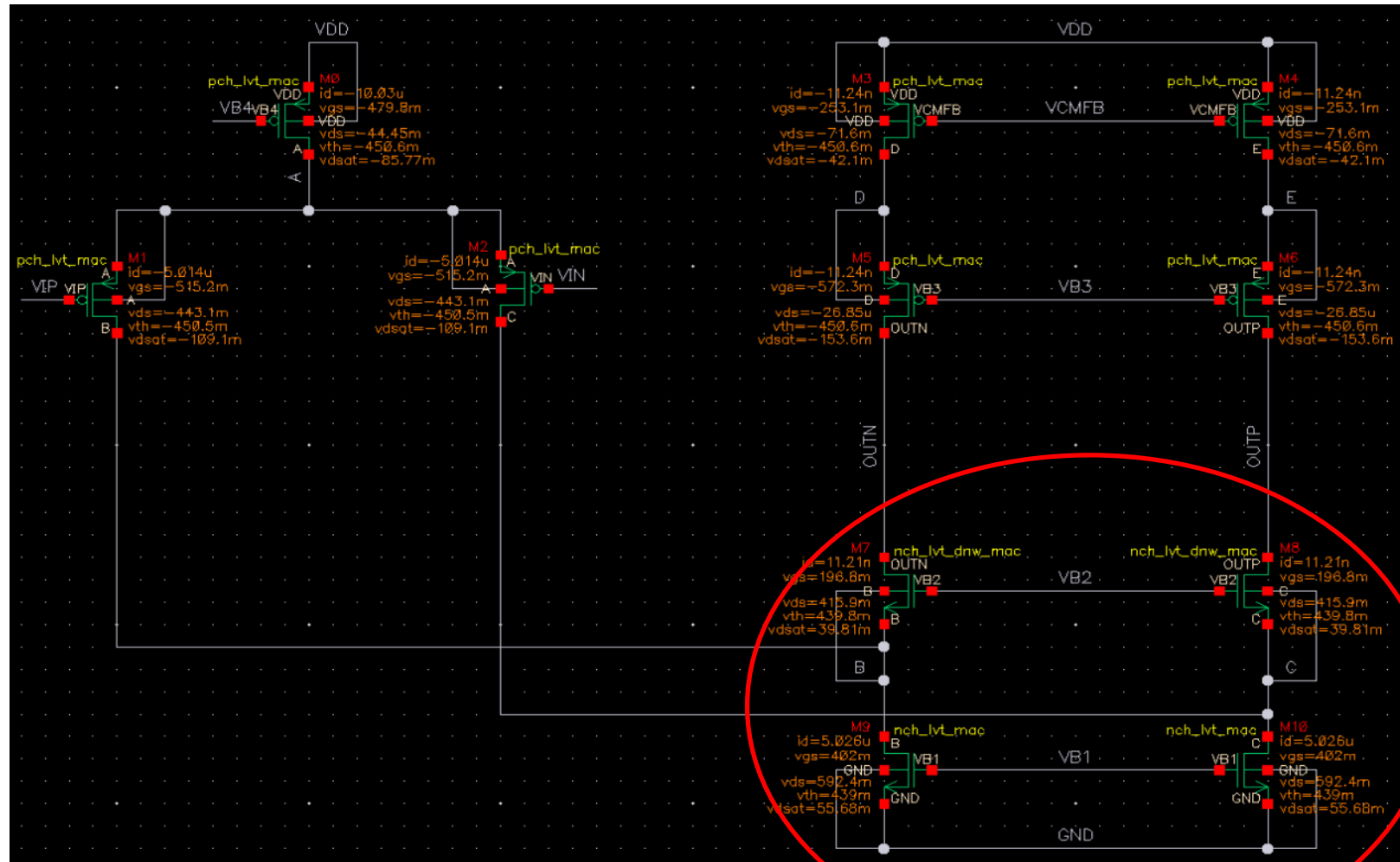
Parameter	C0_9	C0_10	C0_11	C0_12	C0_13	C0_14	C0_15	C0_16	C0_17
Model Group	FF	FF	FF	FF	FF	FF	FF	FF	FF
VDD	1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
temperature	-20	27	80	-20	27	80	-20	27	80

Output	C0_9	C0_10	C0_11	C0_12	C0_13	C0_14	C0_15	C0_16	C0_17
gbw	3.226G	2.835G	2.482G	3.395G	3.026G	2.675G	3.535G	3.175G	2.823G
gain	83.5	79.3	70.98	88.59	83.34	77.66	88.83	84.09	78.85

- N_Aux_Amp: N mos input folded cascade
- P_Aux_Amp: P mos input folded cascade



- P_Aux_Amp: P mos input folded cascode





C0_0	C0_1	C0_2	C0_3	C0_4	C0_5	C0_6	C0_7	C0_8
TT	TT	TT	TT	TT	TT	TT	TT	TT
1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
-20	27	80	-20	27	80	-20	27	80

C0_0	C0_1	C0_2	C0_3	C0_4	C0_5	C0_6	C0_7	C0_8
2.363G	2.227G	2.121G	3.167G	2.897G	2.625G	3.698G	3.424G	3.139G
87.33	84.37	75.49	89.79	88.19	83.13	90.84	89.08	82.93

C0_9	C0_10	C0_11	C0_12	C0_13	C0_14	C0_15	C0_16	C0_17
FF	FF	FF	FF	FF	FF	FF	FF	FF
1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
-20	27	80	-20	27	80	-20	27	80

C0_9	C0_10	C0_11	C0_12	C0_13	C0_14	C0_15	C0_16	C0_17
2.584G	2.313G	2.19G	3.405G	3.129G	2.858G	3.894G	3.622G	3.344G
84.16	80.91	72.6	87.91	86.09	80.81	89.23	87.18	80.04

C0_18	C0_19	C0_20	C0_21	C0_22	C0_23	C0_24	C0_25	C0_26
SS	SS	SS	SS	SS	SS	SS	SS	SS
1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
-20	27	80	-20	27	80	-20	27	80

C0_18	C0_19	C0_20	C0_21	C0_22	C0_23	C0_24	C0_25	C0_26
2.193G	2.11G	2.012G	2.888G	2.618G	2.347G	3.479G	3.201G	2.914G
88.69	85.82	76.65	90.89	89.36	83.82	91.96	90.39	85.01

C0_36	C0_37	C0_38	C0_39	C0_40	C0_41	C0_42	C0_43	C0_44
SF	SF	SF	SF	SF	SF	SF	SF	SF
1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
-20	27	80	-20	27	80	-20	27	80

C0_36	C0_37	C0_38	C0_39	C0_40	C0_41	C0_42	C0_43	C0_44
2.589G	2.334G	2.201G	3.296G	3.037G	2.77G	3.785G	3.521G	3.222G
87.84	82.56	73.57	90.19	87.52	78.32	91.06	88.55	77.07

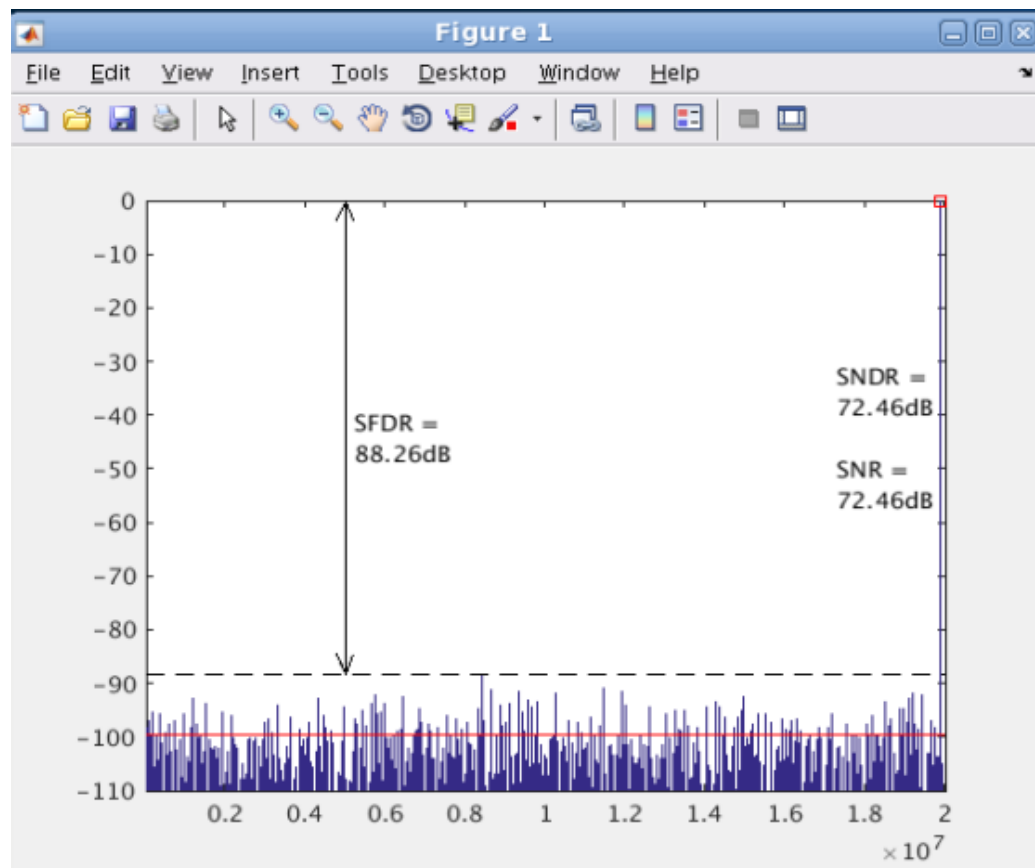
C0_27	C0_28	C0_29	C0_30	C0_31	C0_32	C0_33	C0_34	C0_35
FS	FS	FS	FS	FS	FS	FS	FS	FS
1.08	1.08	1.08	1.2	1.2	1.2	1.32	1.32	1.32
-20	27	80	-20	27	80	-20	27	80

C0_27	C0_28	C0_29	C0_30	C0_31	C0_32	C0_33	C0_34	C0_35
2.053G	2.022G	1.955G	2.972G	2.71G	2.45G	3.6G	3.321G	3.047G
81.32	80.76	74.1	87.78	86.88	83.62	89.97	88.65	84.98

- 45 corner was tested.
- Temperature: {-20,27,80}
- MOS : {TT,SS,FF,SF,FS}
- VDD : 0.9VDD,VDD,1.1VDD

TT, 27, 1.2V with transient noise

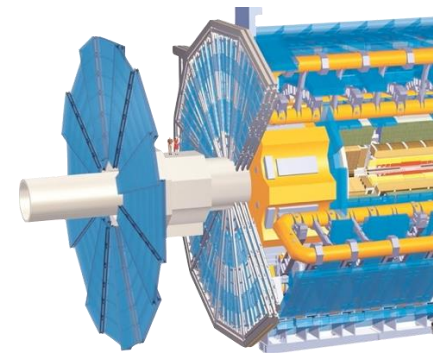
	Power Consumption
VDD	1.2V
Sample Rates	40MS/s
SNDR	72.46dB = 11.74 bits
Power Consumption	3mW



-
- Corner simulation of whole 12-b ADC
 - 12-b Pipeline SAR ADC simulation together with bonding wire.
 - DAC Array layout.



TEXAS
The University of Texas at Austin



UT-Austin ADC Design ATLAS LAr Calorimeter at HL-LHC

Chen-Kai Hsu

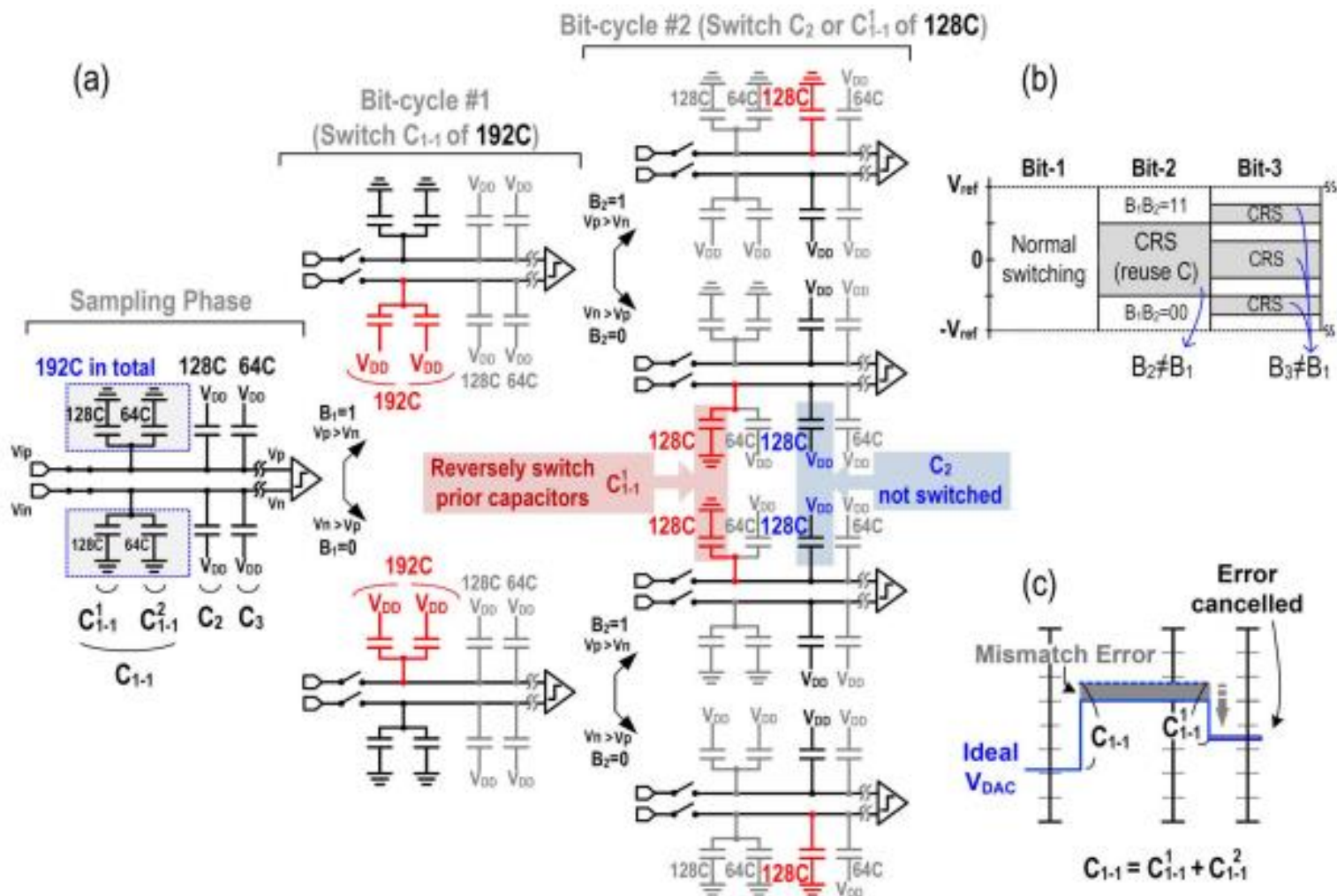
ckhsu@utexas.edu

Nov 22, 2016

-
- Capacitor Linearity Enhancement
 - Implementation Progress
 - Future work

Capacitor Matching Enhancement

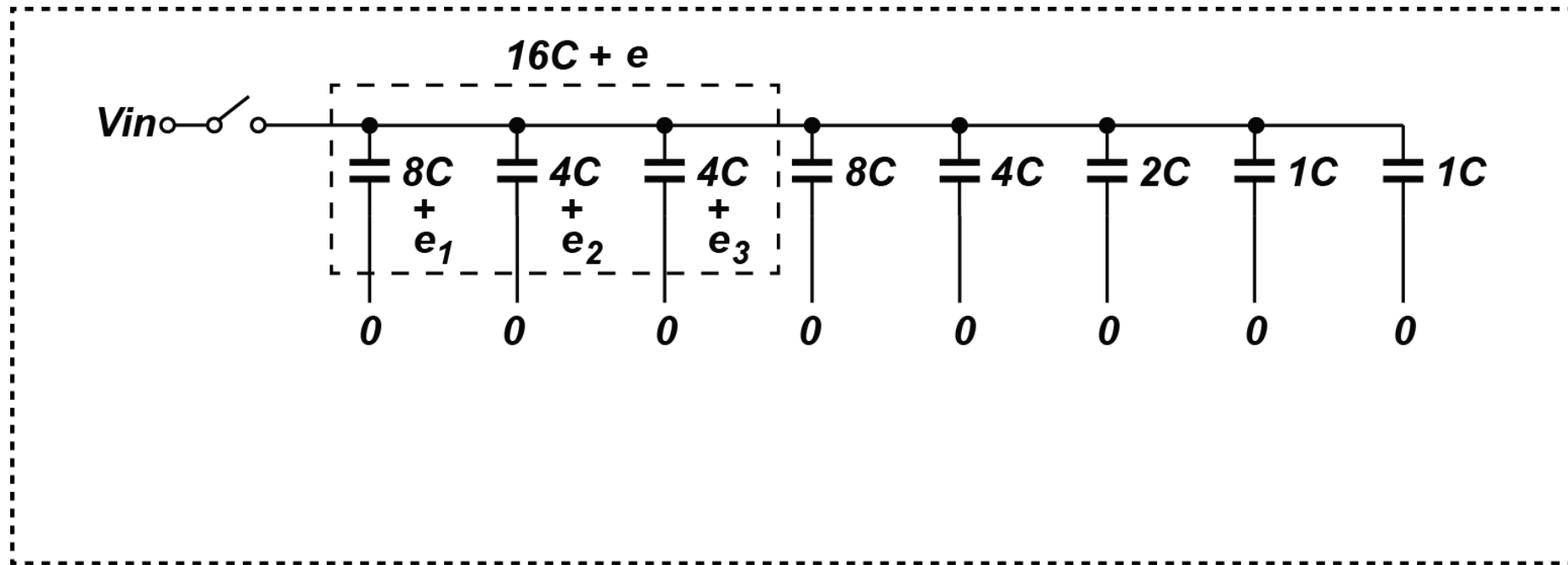
- Reversed Switching, RS, [1] JSSCC'15





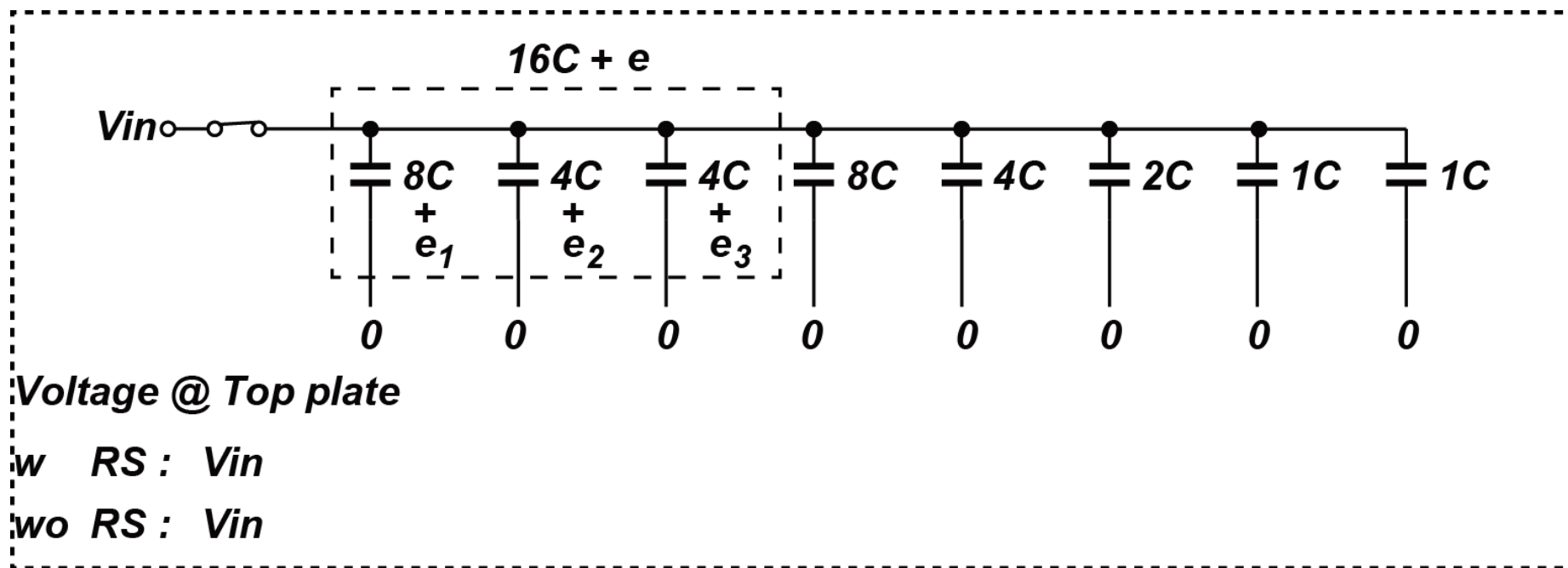
Capacitor Matching Enhancement

- Digital Sequence : 100



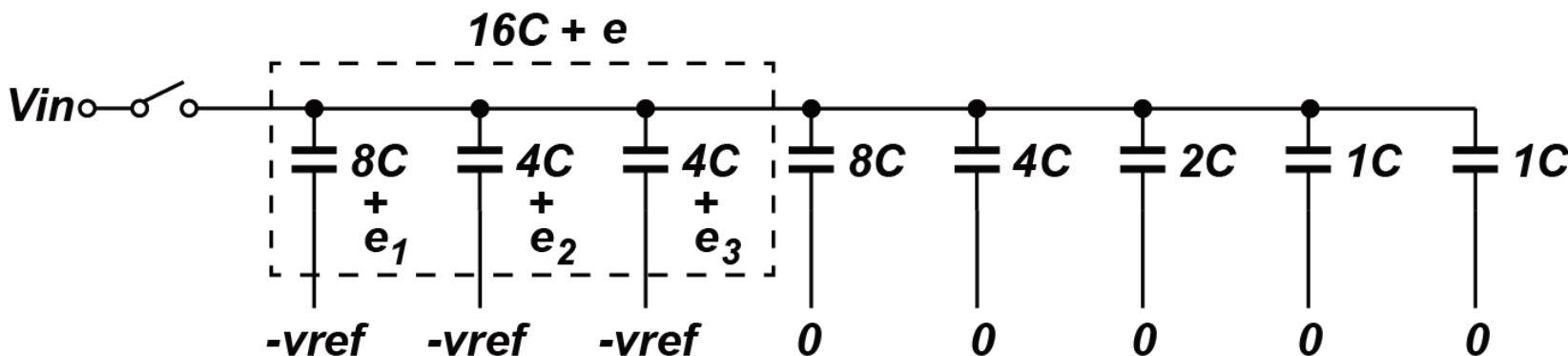
Capacitor Matching Enhancement

- Digital Sequence : 100



Capacitor Matching Enhancement

- Digital Sequence : 100



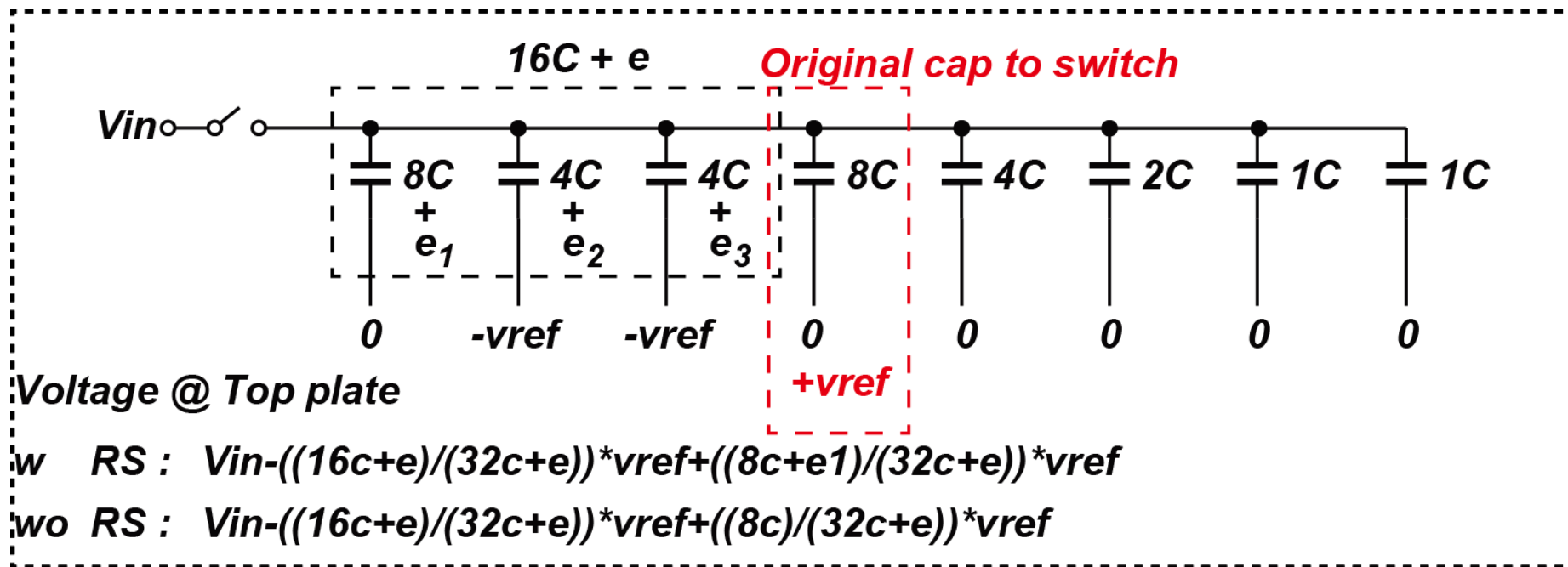
Voltage @ Top plate

With RS : $V_{in} - ((16C + e) / (32C + e)) * v_{ref}$

Without RS : $V_{in} - ((16C + e) / (32C + e)) * v_{ref}$

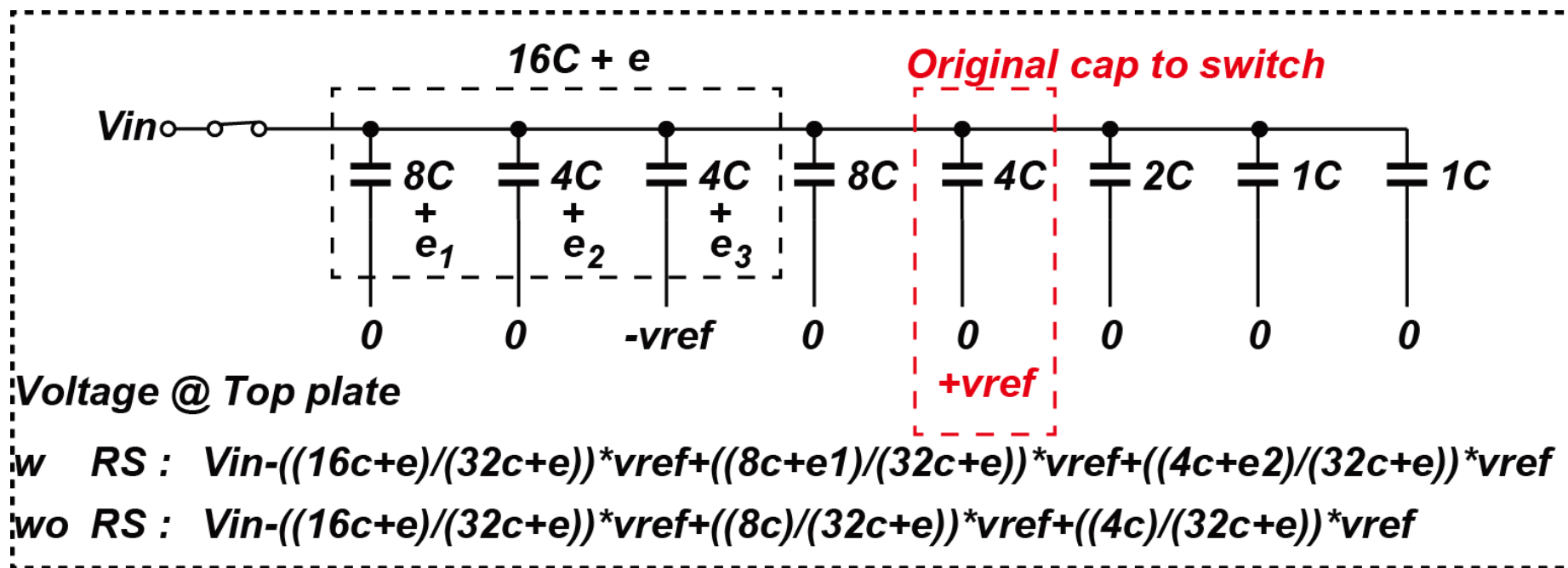
Capacitor Matching Enhancement

- Digital Sequence : 100



Capacitor Matching Enhancement

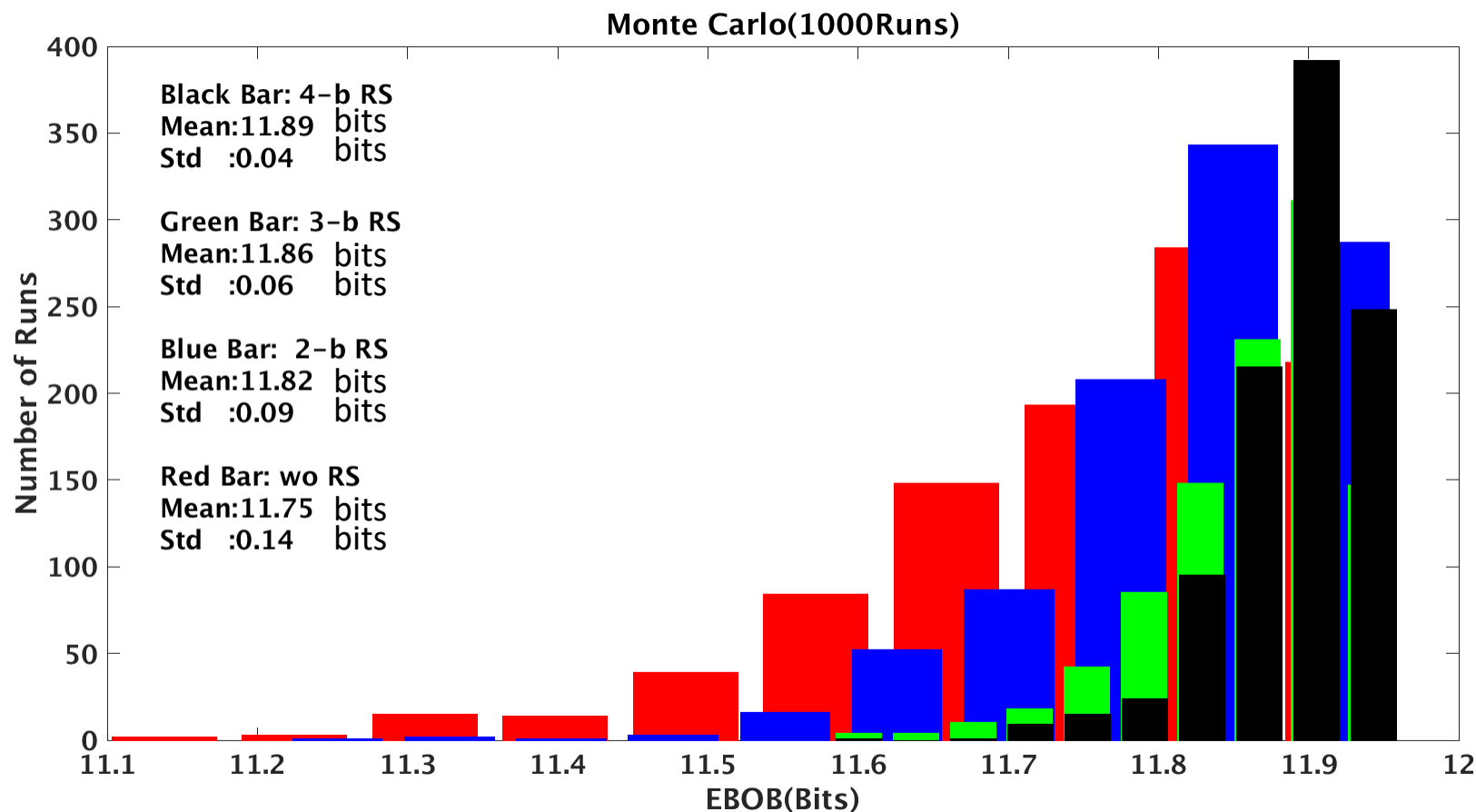
- Digital Sequence : 100



- Remember that e equals to $e_1 + e_2 + e_3$

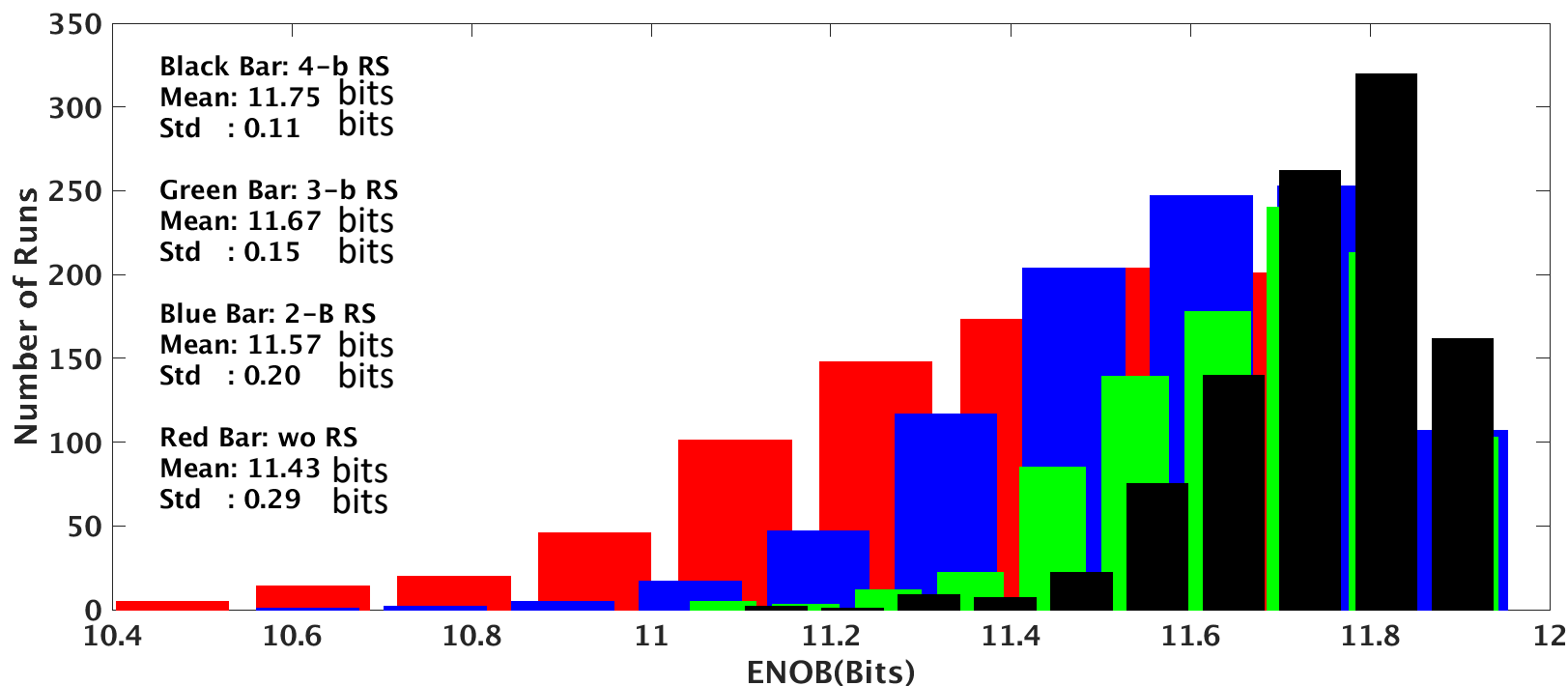
Capacitor Matching Enhancement

- Unit capacitor of 200fF in 1st stage.

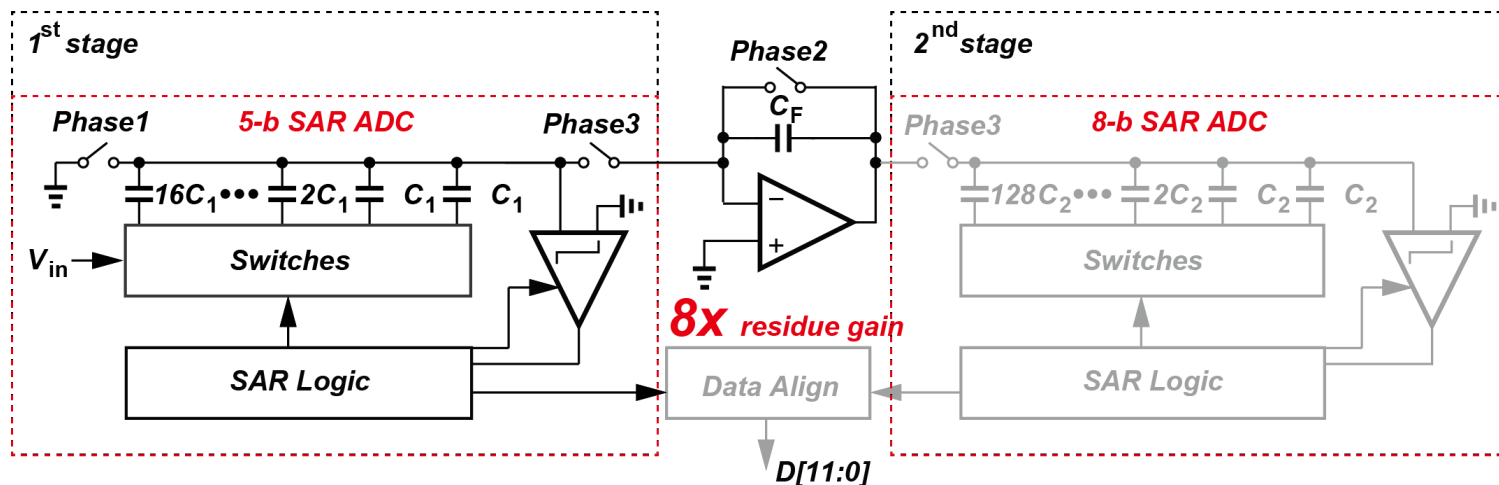


Capacitor Matching Enhancement

- Unit capacitor of 20fF in 1st stage.

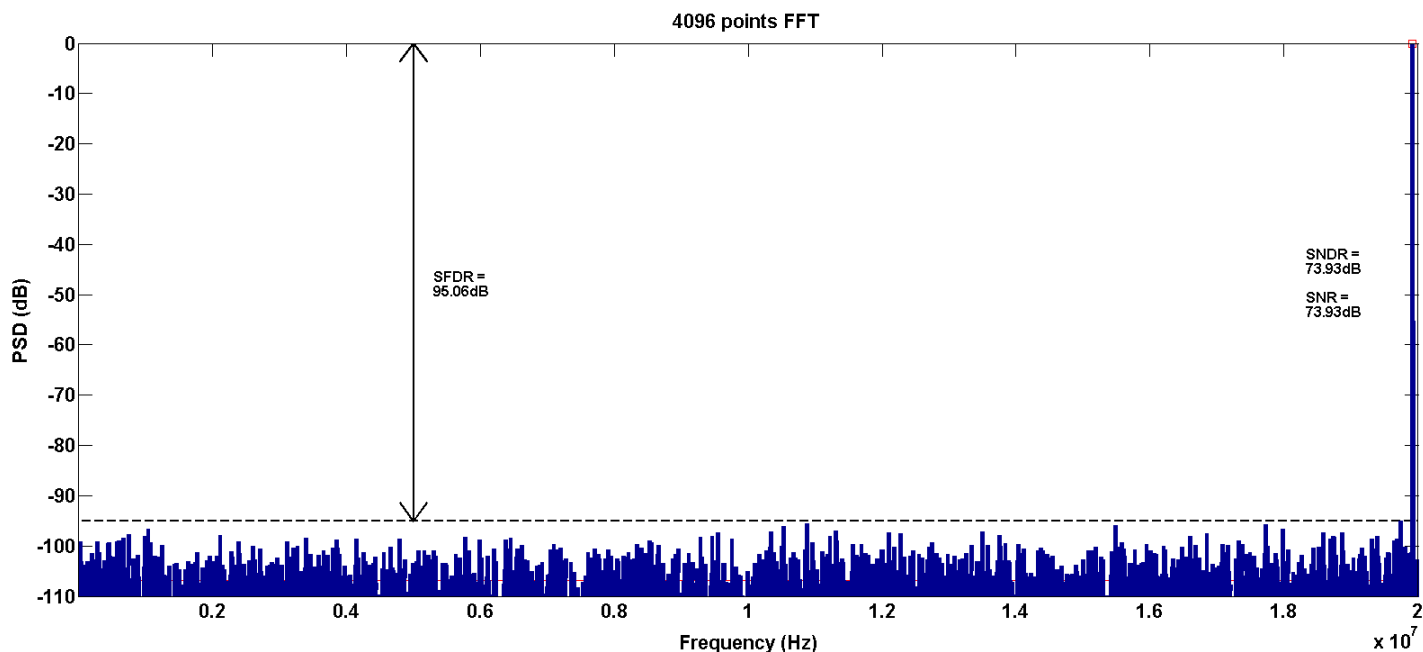
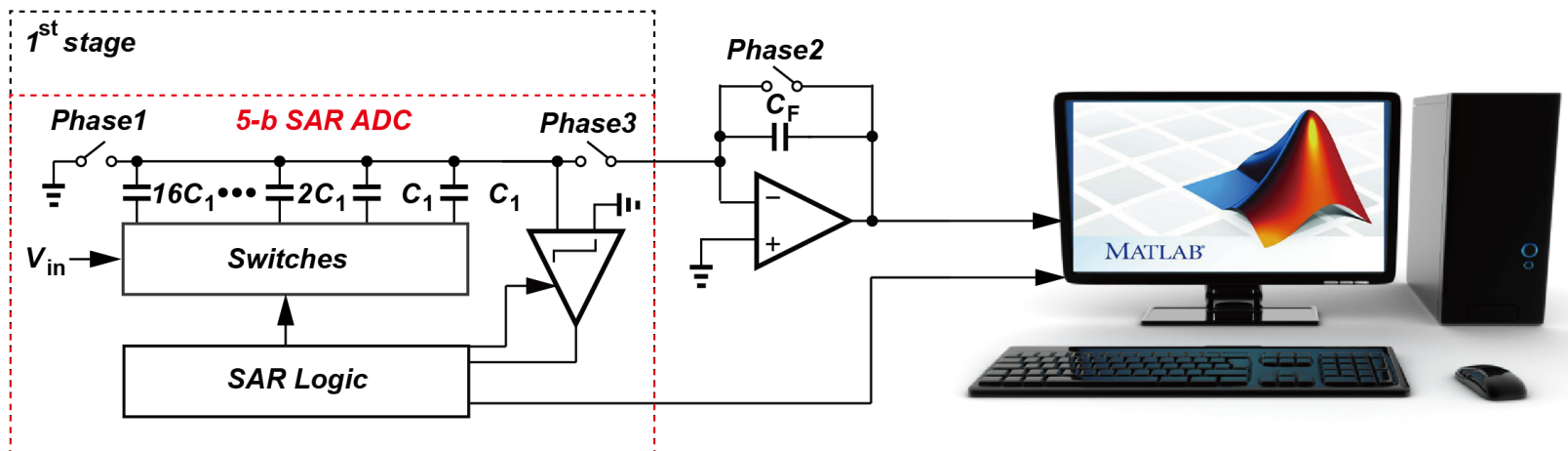


- First stage has been built(without RS).



	Power Consumption
OPAMP	1.8mW
1 st Comparator	60uW
1 st SAR Logic	20uW
Bootstrap Switch	6uW

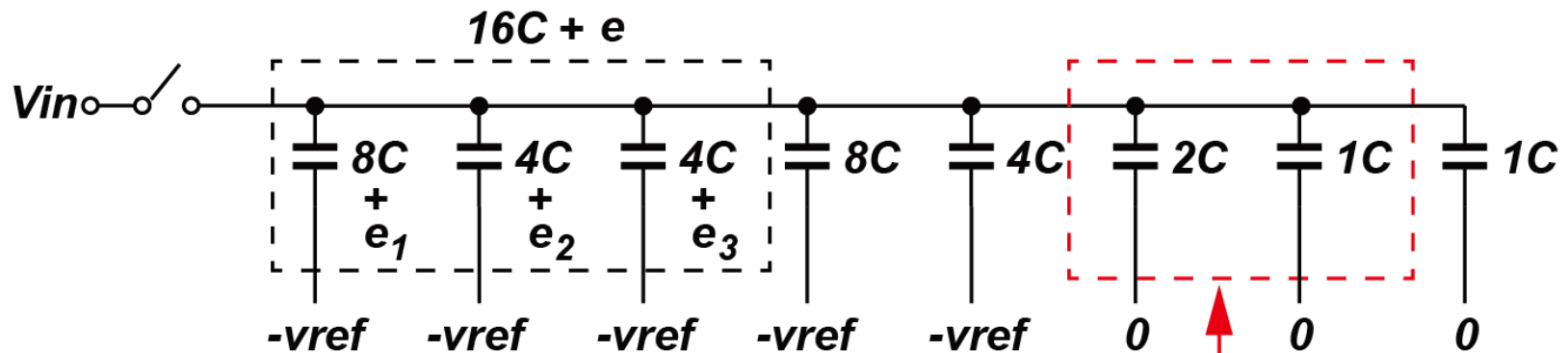
- Feed the residue of amplifier and digital code into Matlab.



-
- Implement the RS technique into the first stage.
 - Doing more simulation on first stage before next meeting, such as corner simulation and noise simulation.

-
1. J.-H. Tsai et al., “A 0.003 mm² 10 b 240 MS/s 0.7 mW SAR ADC in 28 nm CMOS with digital error correction and correlated-reversed switching,” IEEE J. Solid-State Circuits, vol. 50, no. 6, pp. 1382–1398, Jun. 2015.

If the digitized code is 111, the following switching will not switch back.

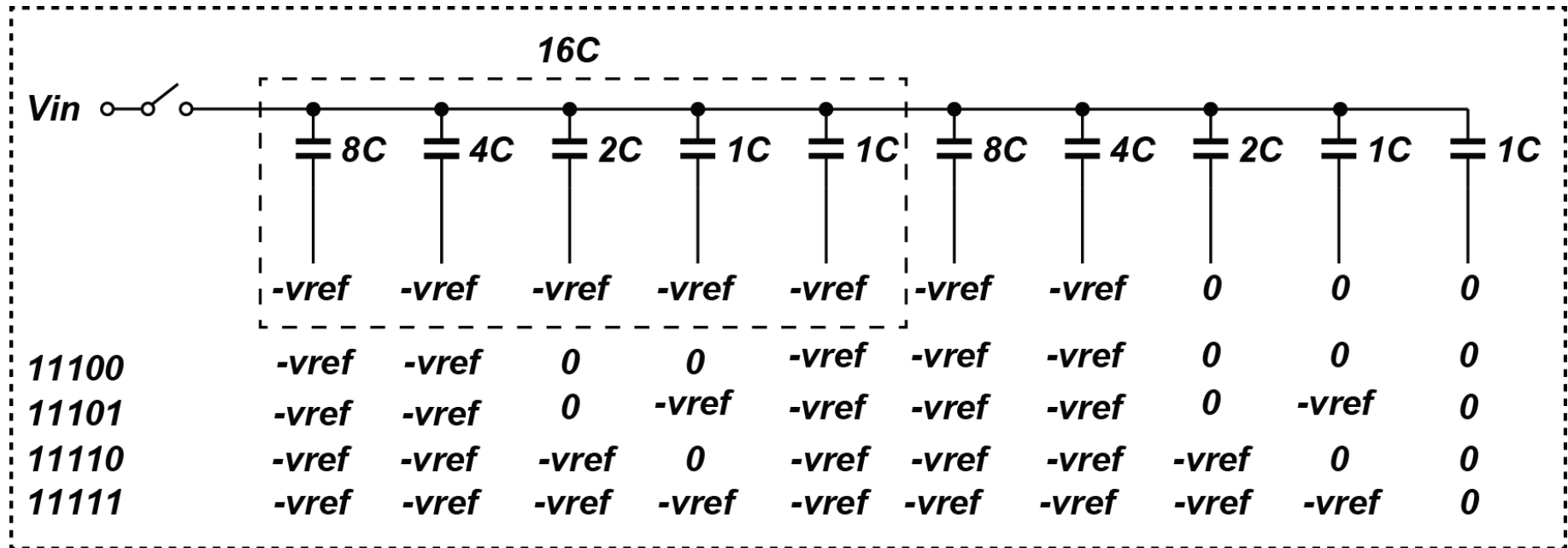


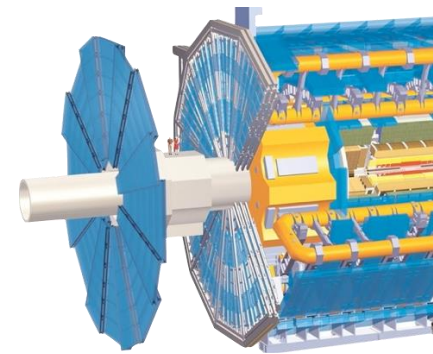
The subsequent switching will switch these two cap

Performing more bits RS will alleviate this dilemma.

Assuming 111 has been resolved and the following sequence will be 00, 01, 10, 11.

Except for 11111, the other sequence will have at least one switching back.





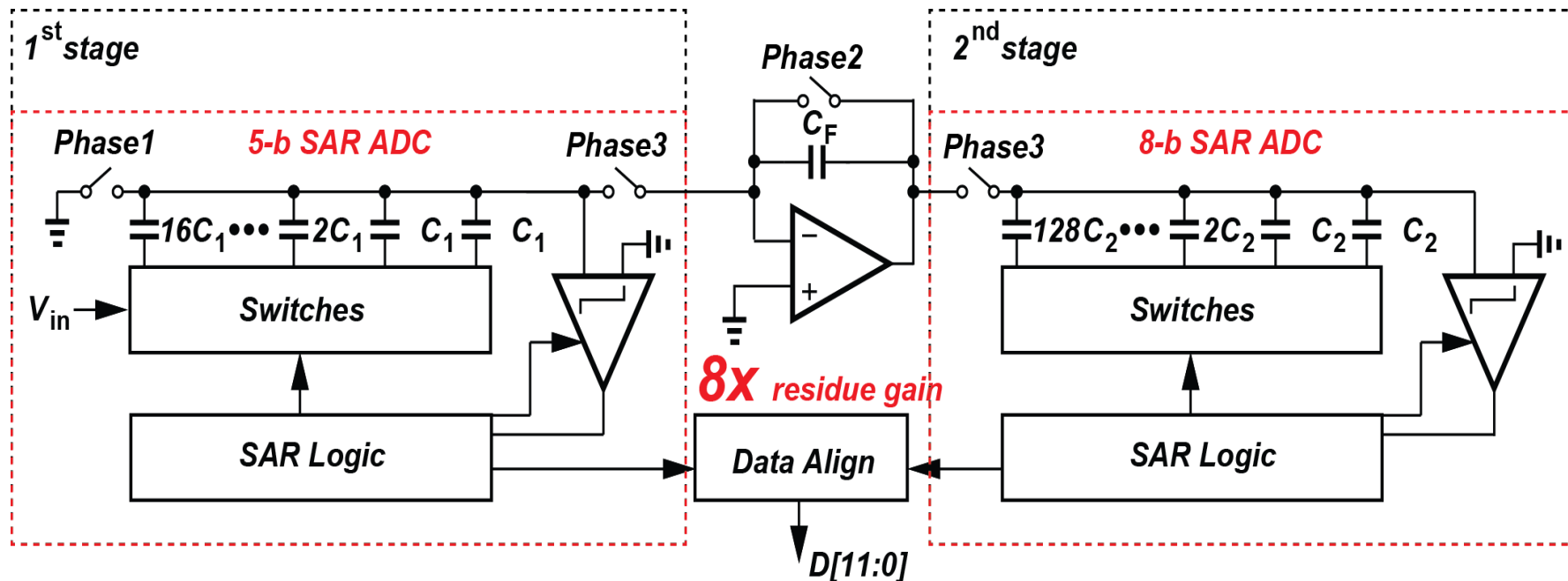
UT-Austin ADC Design ATLAS LAr Calorimeter at HL-LHC

Chen-Kai Hsu

ckhsu@utexas.edu

Nov 4, 2016

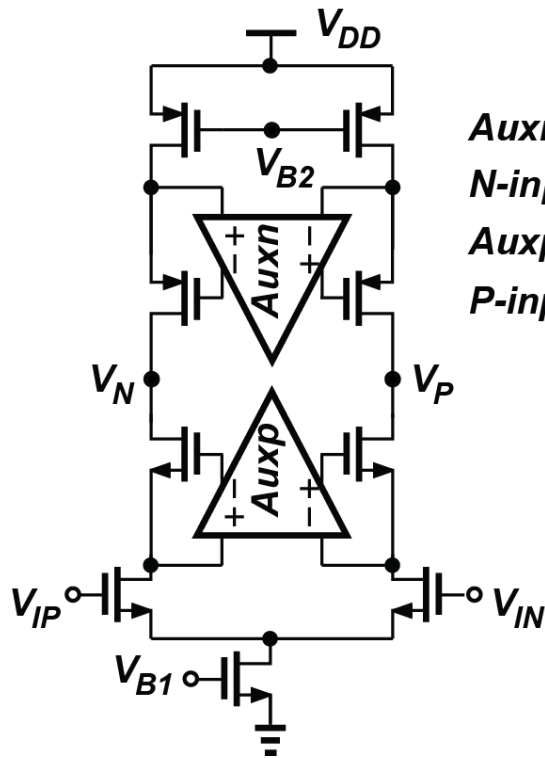
What about 8x inter-stage gain ?



Open-Loop Gain can be reduced from 78dB to 72dB.

Unit-Gain Bandwidth can be reduced from 1.27GHz to 635MHz.

Due to **reduced swing**, maybe we can just use telescopic with gain boosting(One-stage which means **low power**).

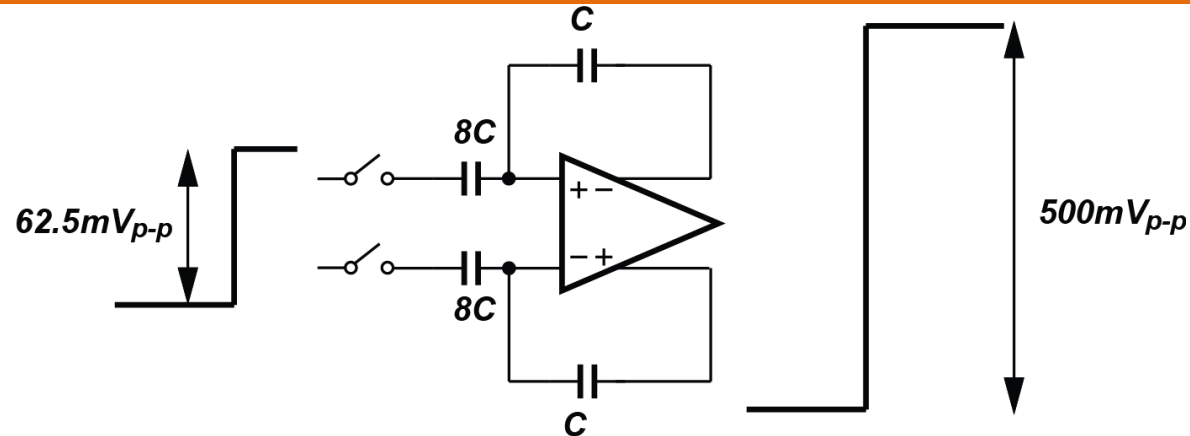


Auxn:
N-input Folded Cascode
Auxp:
P-input Folded Cascode

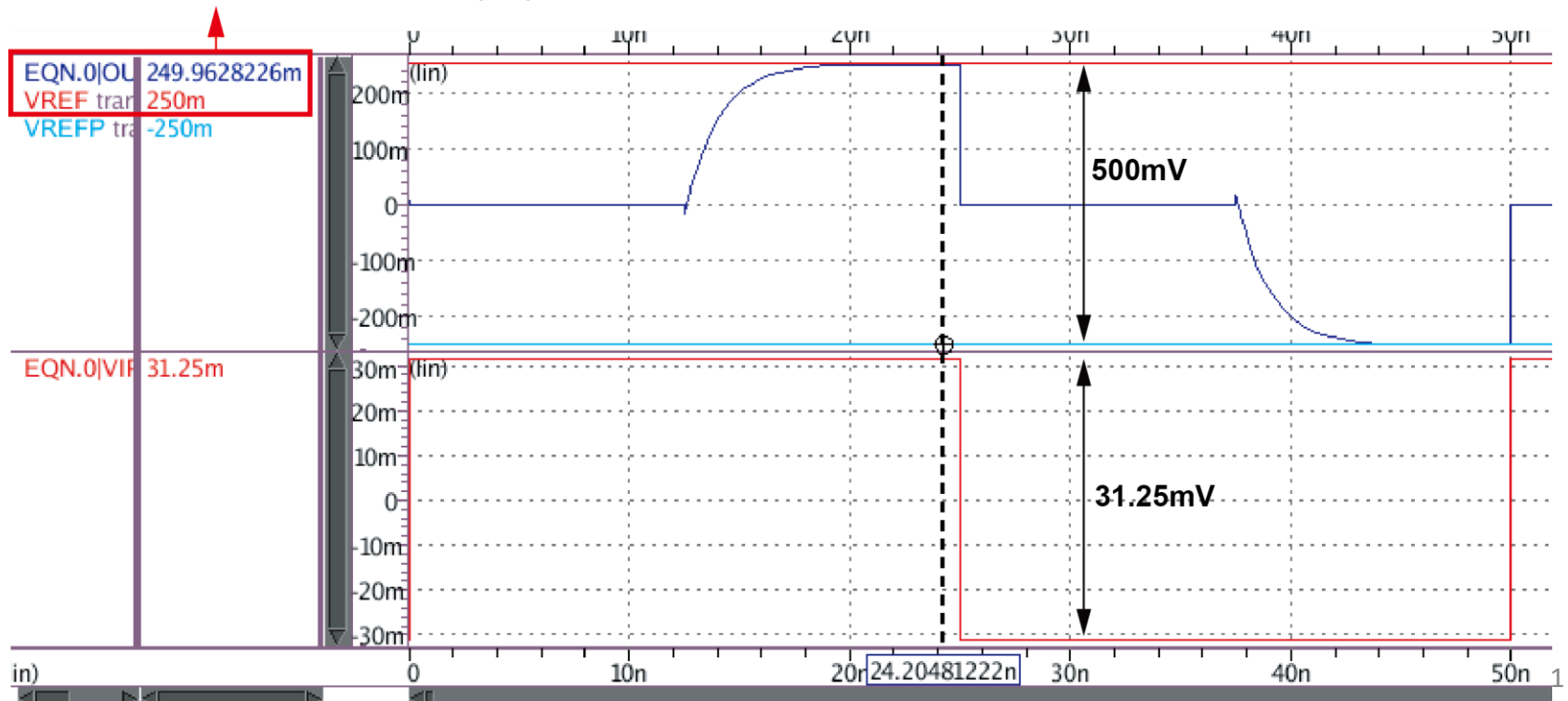
	Specification
Supply Voltage	1.2 V
Technology	TSMC 65LP 1P6M
DC Gain	80dB
Current-Main	750uA
Current-Auxn	100uA
Current-Auxp	100uA
Bias Circuit	200uA
PhaseMargin	80 degree
Unit-Gain Freq	2.1GHz

- According to [1], the frequency response of this opamp has to be carefully designed to ensure stability and to avoid pole-zero doublet, causing slow settling.
- $\beta\omega_{main,ta} < \omega_{aux,ta} < \omega_{main,2n\ pole}$

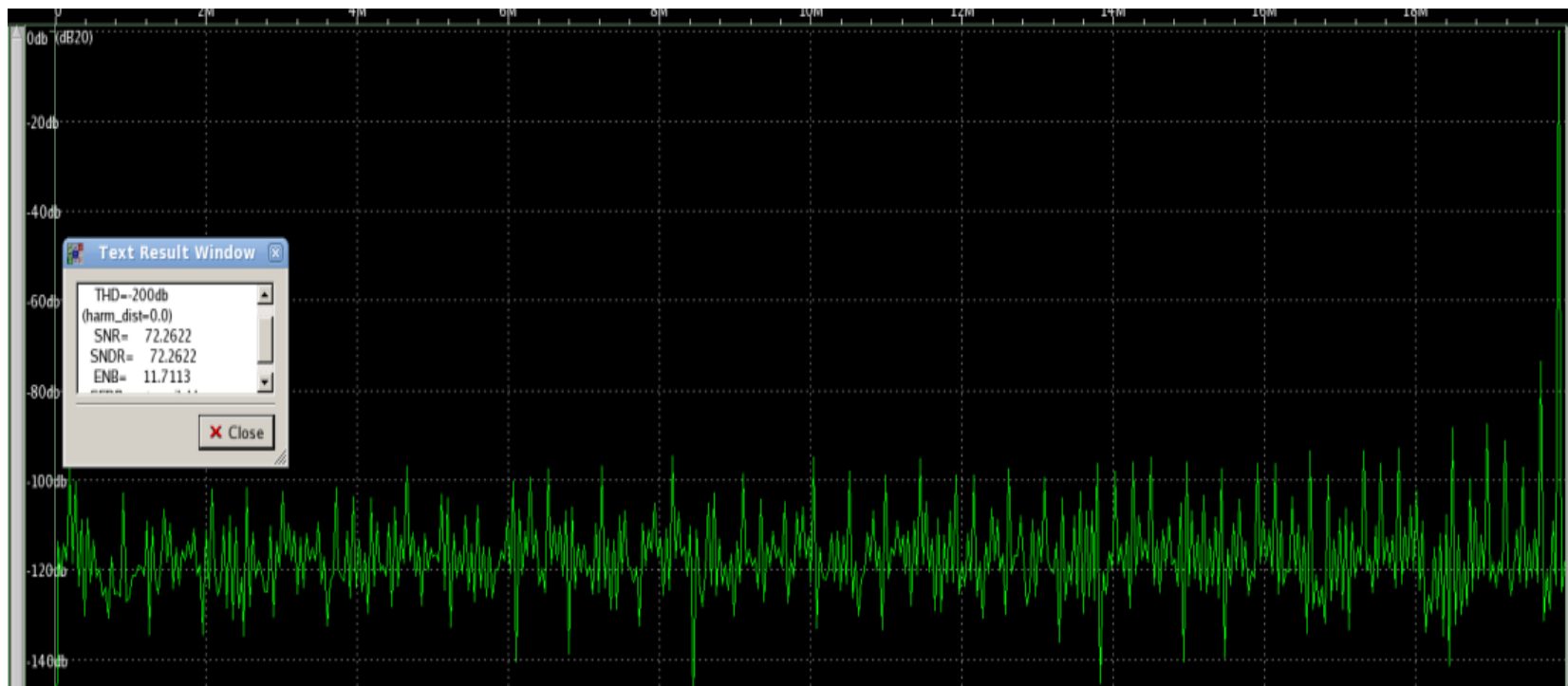
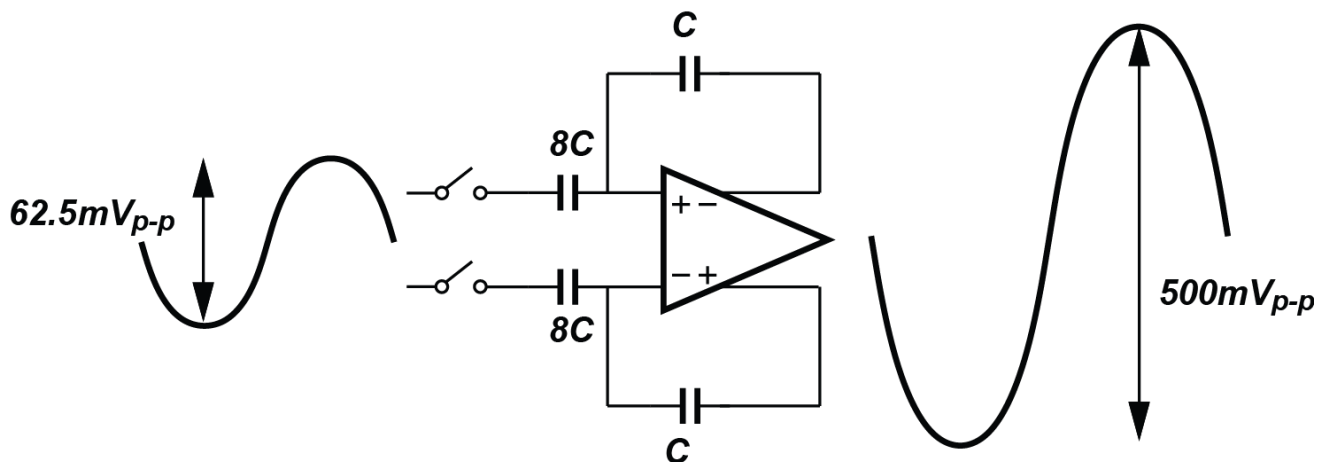
Step Response



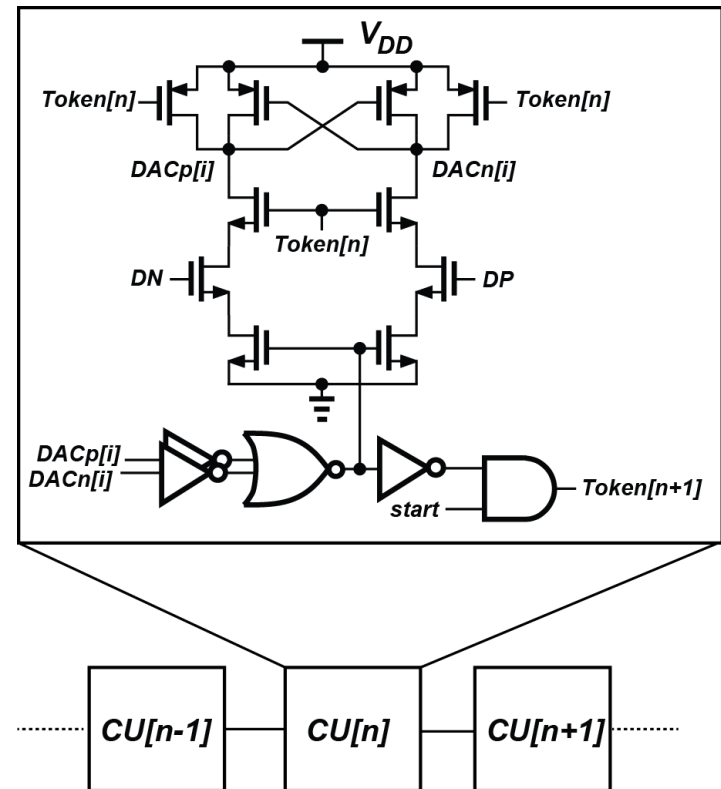
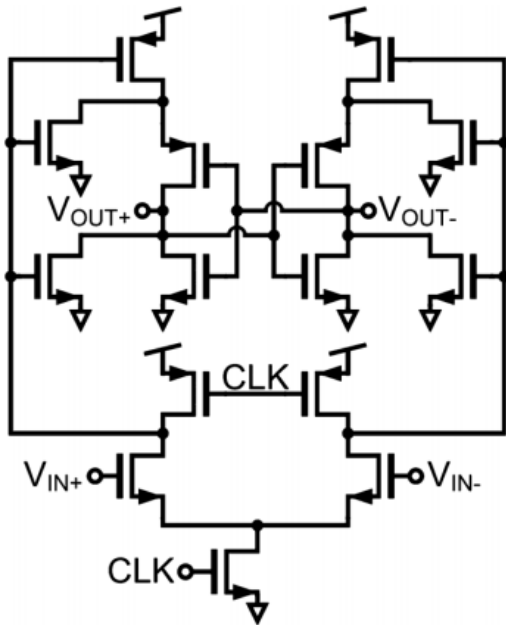
$$\text{Error} = 250\text{m} - 249.96\text{m} = 0.04\text{m} < (0.5)/2^9$$



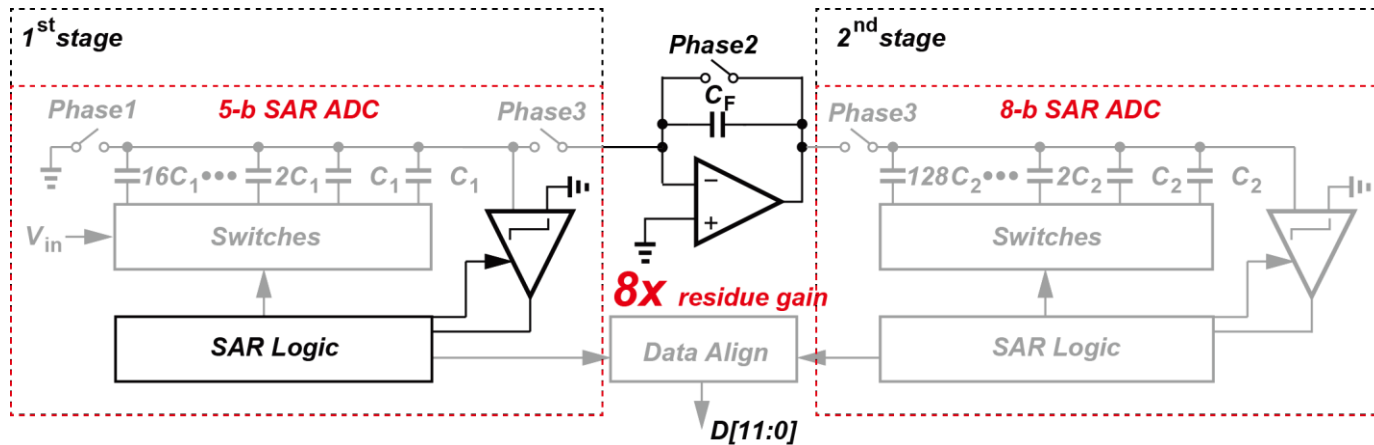
Linearity Test



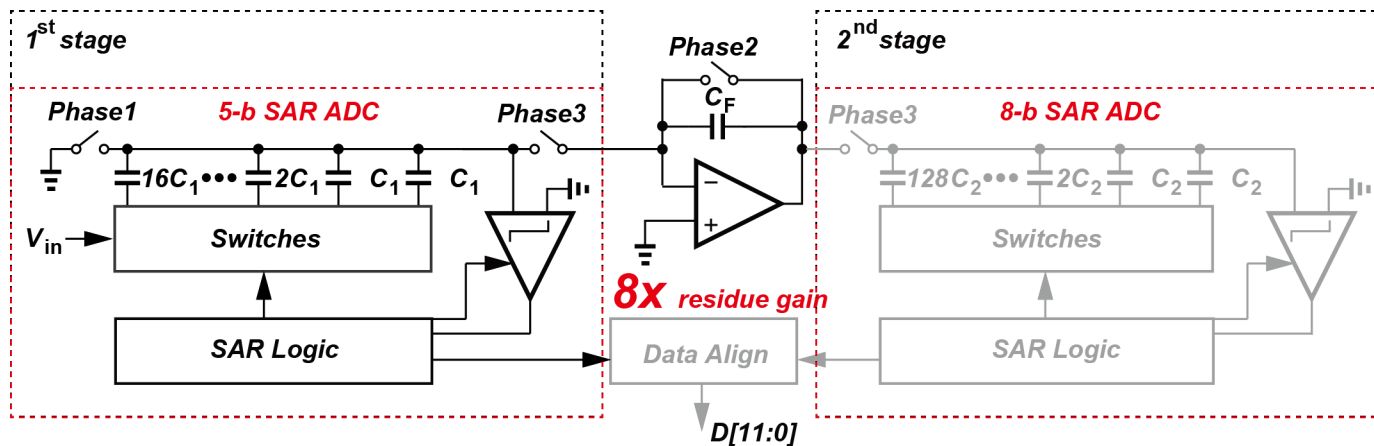
- [2] ISSCC' 15
- Low noise single phase dynamic latched comparator
- [3] VLSI'11
- Direct switching



- Things have been done:

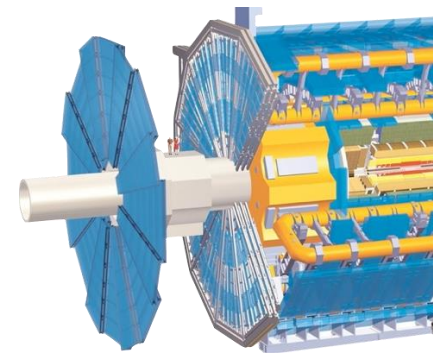


- Future Plan(in the near 1 to 2 weeks):



	[4] ESSCIRC'16	[2] ISSCC'15
Architecture	Noise Shaping SAR ADC	Pipeline SAR ADC
Technology	130 nm	65 nm
DAC Calibration	No	No
Total capacitance	2.1 pF	2.048 pF
SNDR	74 dB	70.9 dB
SFDR	95 dB	84.6 dB

1. K. Bult and G. J. G. M. Geelen, “A fast-settling CMOS Op Amp for SC circuits with 90-dB dc gain,” ***IEEE J. Solid-State Circuits***, vol. 25, pp.1379–1384, Dec. 1990.
2. Y. Lim and M. P. Flynn, “A 1 mW 71.5 dB SNDR 50 MS/S 13b fully differential ring-amplifier-based SAR-assisted pipeline ADC,” ***in Proc. IEEE ISSCC. Dig. Tech. Papers***, Feb. 2015, pp. 1–3.
3. J.-H. Tsai, Y.-J. Chen, M.-H. Shen and P.-C. Huang, “A 1-V, 8b, 40MS/s, 113 μ W Charge-Recycling SAR ADC with a 14 μ W Asynchronous Controller,” ***Symp. on VLSI Circuits***, pp. 264-265, June 2011.
4. Wenjuan Guo, and Nan Sun , “A 12b-ENOB 61 μ W noise-shaping SAR ADC with a passive integrator ,” ***ESSCIRC***, pp. 405-408, Oct. 2016.



UT-Austin ADC Design ATLAS LAr Calorimeter at HL-LHC

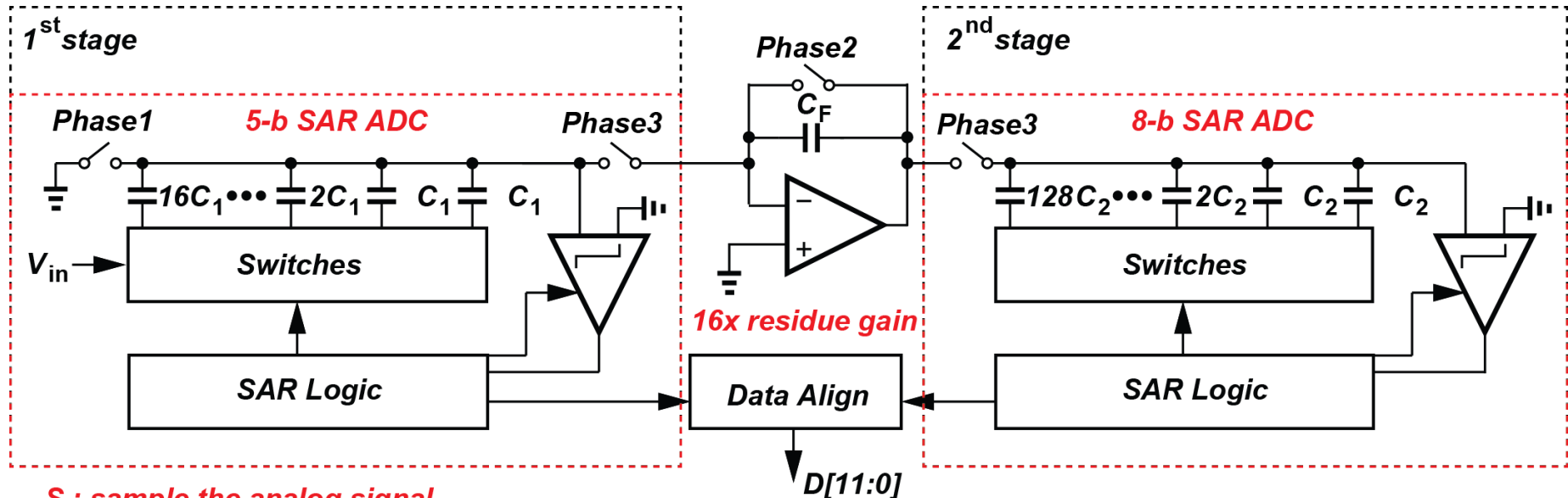
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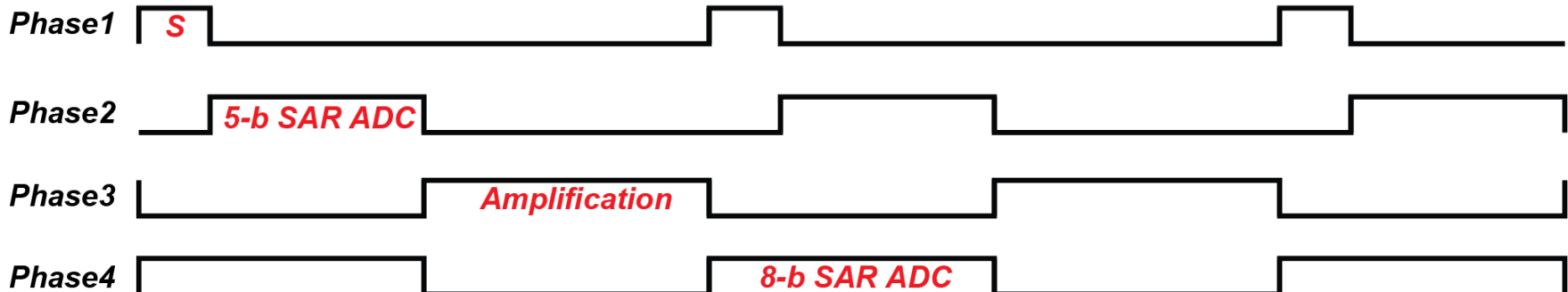
October 7, 2016

- Education
 - M.S., National Taiwan Univ., 2015
 - B.S., National Chung Cheng Univ., 2012.
- First year PhD student at UT Austin.
- My research interests include high-performance data converters, sensor interface, and mixed-signal circuits
- Process experience:
 - CMOS 0.18 μ m / 90nm / 40nm.
- Some Research experience:
 - Low-power high-speed Pipeline ADC in 90-nm technology.
 - Low-power SAR ADC in a 0.18- μ m technology for smart badge.
- Publication:
 - **Chen-Kai Hsu** and Tai-Cheng Lee, “A Single-Channel 10-b 400-MS/s 8.7-mW Pipeline ADC in a 90-nm Technology.” *IEEE Asian Solid-State Circuits Conf. Dig. Tech. Papers*, pp. 233-236, Xiamen, China, Nov. 2015.

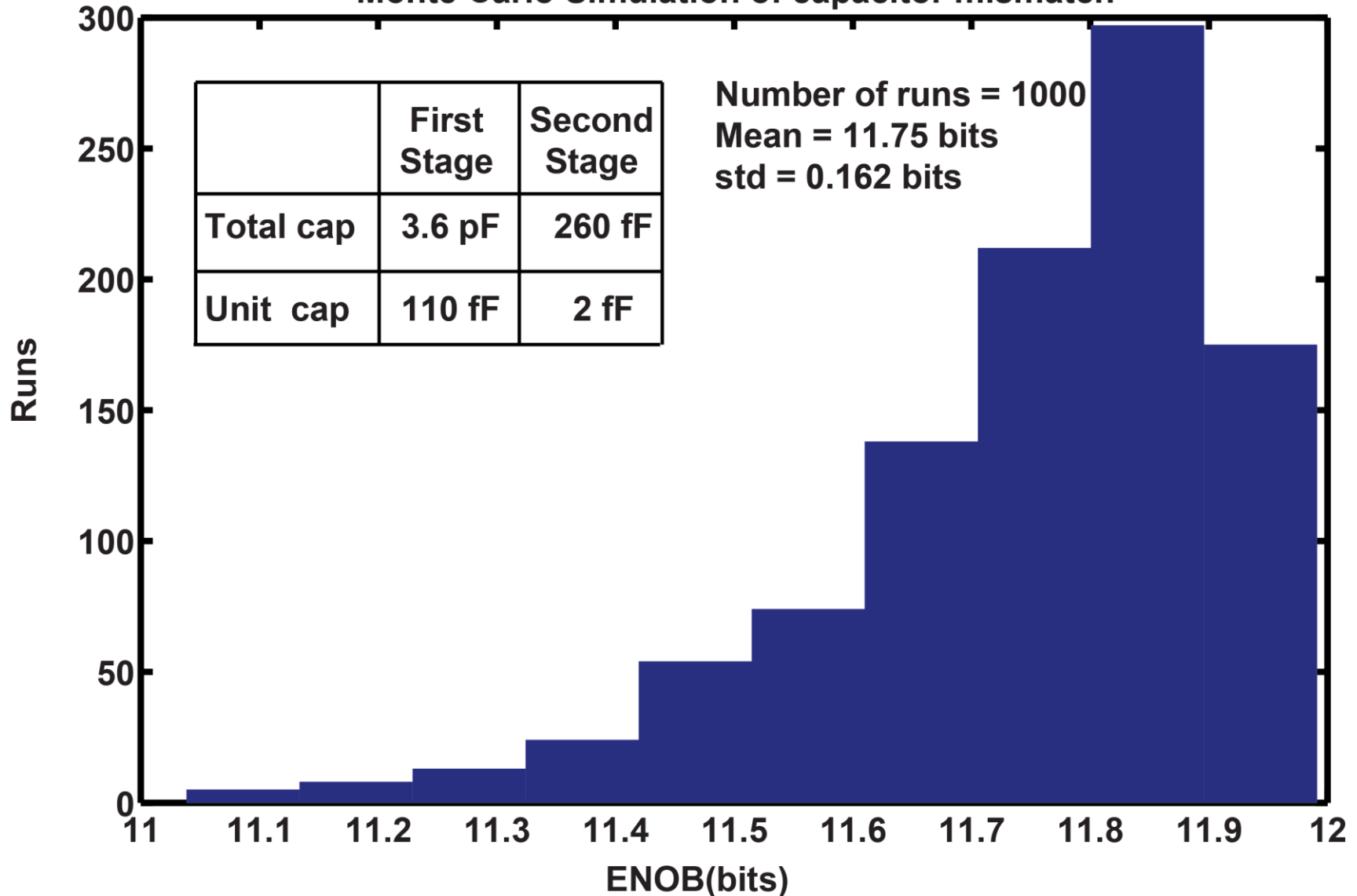
The ADC is a 5 + 8 bit two-step structure with 1 bit inter stage redundancy to generate a 12-bit output.



S : sample the analog signal



Monte Carlo Simulation of capacitor mismatch





- **Open-loop gain consideration:**

By charge conservation, the output of a residue amplifier can be derived as:

$$V_{RES} \approx \frac{32C_1}{C_F} (VIN - \frac{1}{32} (16B_1 + 8B_2 + \dots + B_5)V_{REF})(1 - \text{Error})$$

$$\text{Where Error} = \frac{32C_1 + C_P + C_F}{AC_F}$$

Therefore, in order to provide **16x** close-loop gain, we need a **78dB** open-loop gain amplifier to satisfy 8-b accuracy(1/2LSB).

- **Bandwidth consideration:**

Assuming amplifier is a single pole system, we have:

$$V_{RES} = V_{STEP}(1 - e^{-t/\tau}) \quad \tau = \frac{1}{\omega_{3dB}}$$

At least, 1.27GHz unit-gain bandwidth is needed.



Assuming 2 stage Miller compensated OTA:

$$\text{Phase Margin} = 90^\circ - \arctan\left(\frac{g_{m1}/C_C}{g_{m2}/C_L}\right);$$

$$g_m = \frac{I_{tail}}{V_{overdrive}}$$

For Phase Margin at least greater than 65 degree,

- $I_{stage2} = I_{stage1} \Rightarrow C_C = 2.2C_L$ (V_{eff} are the same at each stage)
- $C_L = 260\text{fF}$ (decided by monte carlo simulation). $\Rightarrow C_C = 572\text{fF}$
- $g_m = 2 * \pi * 1.27\text{GHz} * C_C = 4.5\text{mS}$
- So, $I_{stage2} = I_{stage1} = 0.45\text{mA}$ (assume $V_{overdrive} = 0.1\text{ V}$)

Power estimation of this work	
Total	> 3.6 mW
Amplifier	> 1.08 mW
Ref. buffer	2 mW
others	0.9 mW

*others include
 1.digital circuit
 2.bootstrap switch
 3.clock buffer

	This work	(1) VLSI 2010
Architecture	Pipeline SAR	Pipeline SAR
Calibration	No	No
Technology	TSMC 65 nm	65 nm
Resolution	12 bits	12 bits
Supply Voltage	1.2 V	1.3 V
Sampling Frequency	40 MHz	50 MHz
ENOB	> 11.2 bits	10.7 bits
Power	> 3.6mW	* 3.5mW
Input Range(diff.)	2 Vp-p	2 Vp-p

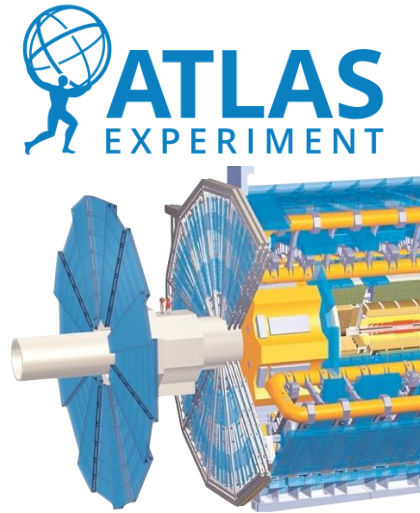
* Power excluding reference buffer

	Specification	Confidence
Technology	TSMC 65 nm	OK
Supply Voltage	1.2 V	OK
Sampling Frequency	40 MHz	OK
ENOB	11.2 bits	a little tough
Power	< 20 mW	OK
Input Range	2 Vp-p	OK

Expected Timeline before tapeout

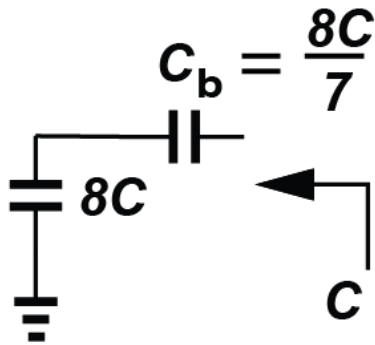
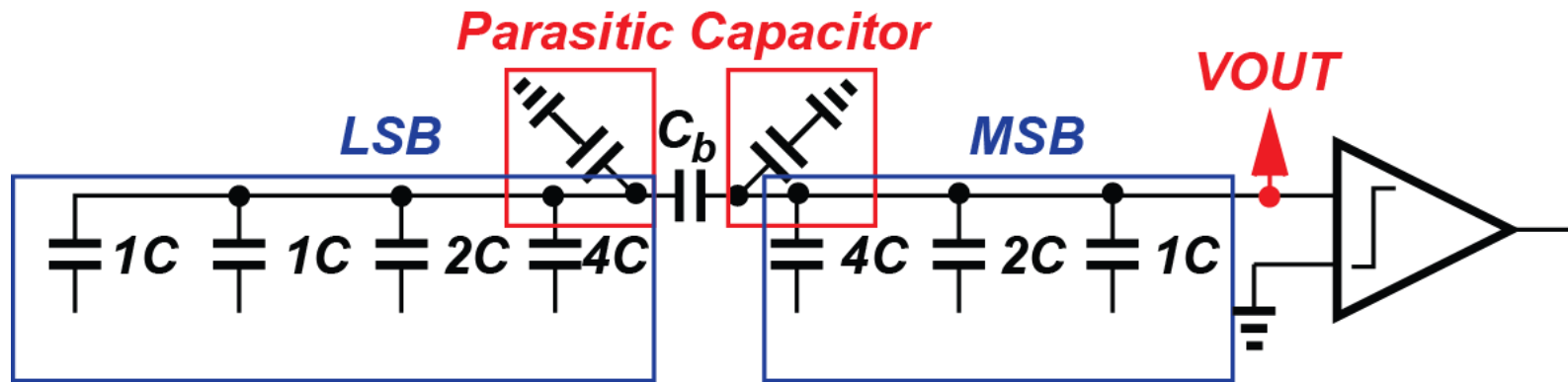
Oct. '16	Nov. '16	Dec. '16	Jan. '17	Feb. '17 to Apr. '17
Amplifier Design	Stage1 Design	Stage2 Design	Whole chip Optimization	Layout and post-simulation

-
1. C. C. Lee and M. P. Flynn, “A SAR-assisted two-stage pipeline ADC,” *IEEE J. Solid-State Circuits*, vol. 46, no. 4, pp. 859–869, Apr. 2011.



Back up slides

1. Bridge Capacitor Array



Hybrid DAC

